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## Globe and Ball Valves

# Selecting Valves: Globe vs. Ball 

The control valve is the most important single element in any fluid handling system, because it regulates the flow of fluid to the process. To properly select a control valve, a general knowledge of the process and components is usually necessary. This reference section can help you select and size the control valve that most closely matches the process requirements.

The sizing of a valve is very important if it is to render good service. If it is undersized, it will not have sufficient capacity. If it is oversized, the controlled variable may cycle, and the seat, and plug will be subject to wire drawing because of the restricted opening.

Systems are designed for the most adverse conditions expected (i.e., coldest weather, greatest load, etc.). In addition, system components (boiler, chiller, pumps, coils, etc.) are limited to sizes available and frequently have a greater capacity than system requirements. Correct sizing of the control valve for actual expected conditions is considered essential for good control.

## A basic rule of control valve sizing is:

The higher the percentage of drop across the wide open valve in relation to the percentage of pressure drop through the line and process coil, the better the control.

## Technical Comparison Between Globe and Ball Valves

Technically, the globe valve has a stem and plug, which strokes linearly, commonly referred to as "stroke" valves. The ball valve has a stem and ball, which turns horizontally, commonly referred to as "rotational" valves.

Early ball valves used a full port opening, allowing large amounts of water to pass through the valve. This gave HVAC controls contractors the ability to select a ball valve two to three pipe sizes smaller than the piping line size. Compared to traditional globe valves that would be only one pipe size smaller than the line size, this was often a more cost-effective device-level solution. In addition, the ball valve could be actuated by a damper actuator, rather than expensive box-style "Mod" motors.

## Pricing Comparison

Today, with equivalent pricing between ball and globe valves, the full port ball valve is falling out of favor for most HVAC control applications. This is also due to its poor installed flow characteristic that leads to its inability to maintain proper control. New "flow optimized" or characterized ball valves, specifically designed for modulating applications, have been developed. Characterized ball valves are sized the same way as globe valves. They provide an equal percentage flow characteristic, enabling stable control of fluids. Additionally, there are more cost-effective valve actuators now available for globe valves. Better control and more-competitive pricing now puts globe valves on the same playing field as characterized ball valves.

## Selection Guidelines

## Globe Valve

- High differential pressure across valve
- Rebuilding of the valve is desired
- Better control performance
- Better low flow (partial load) performance
- Use for steam, water or water/glycol media
- Smaller physical profile than a comparable ball valve


## Characterized Ball Valve

- Tight shutoff or high close offs of around $100 \mathrm{psi}^{*}$ are required
- Isolation or two position control**
- Use for water or water/glycol solution only

[^0]
## Sizing

## Pressure Drop for Water Flow

A pressure drop must exist across a control valve if flow is to occur. The greater the drop, the greater the flow at any fixed opening. The pressure drop across a valve also varies with plug position - from minimum when fully open, to $100 \%$ of the system drop when fully closed.

To size a valve properly, it is necessary to know the full flow pressure drop across it. The pressure drop across a valve is the difference in pressure between the inlet and outlet under flow conditions. When it is specified by the engineer and the required flow is known, the selection of a valve is simplified. When this pressure drop is not known, it must be computed or assumed.

If the pressure drop across the valve when fully open is not a large enough percentage of the total system drop, there will be little change in fluid flow until the valve actually closes, forcing the valve's characteristic toward a quick opening form.

Figure 1 shows flow-lift curves for a linear valve with various percentages of design pressure drop. Note the improved characteristic as pressure drop approaches $100 \%$ of system pressure drop at full flow.

It is important to realize that the flow characteristic for any particular valve, such as the linear characteristic shown in Figure 1 is applicable only if the pressure drop remains nearly constant across the valve for full stem travel. In most systems, however, it is impractical to take $100 \%$ of the system drop across the valve.

A good working rule is, "at maximum flow, 25 to $50 \%$ of the total system pressure drop should be absorbed by the control valve." Although this generally results in larger pump sizes, it should be pointed out that the initial equipment cost is offset by a reduction in control valve size, and results in improved controllability of the system. Reasonably good control can be accomplished with pressure drops of 15 to $30 \%$ of total system pressures. A drop of $15 \%$ can be used if the variation in flow is small.

## Recommended Pressure Drops for Valve Sizing - Water

1. With a differential pressure less than 20 psi, use a pressure drop equal to 5 psi.
2. With a differential pressure greater than 20 psi , use a pressure drop equal to $25 \%$ of total system pressure drop (maximum pump head), but not exceeding the maximum rating of the valve.

## Pressure Drop for Steam

The same methodology should be applied for selecting a valve for steam with the most important consideration is the pressure drop.

First, the correct maximum capacity of the coil must be determined. Ideally, there should be no safety factor in this determination and it should be based on the actual BTU heating requirements. The valve size must be based on the actual supply pressure at the valve. When the valve is fully open, the outlet pressure will assume a valve such that the valve capacity and coil condensing rate are in balance. If this outlet valve pressure is relatively large (small pressure drop), then as the valve closes, there will be no appreciable reduction in flow until the valve is nearly closed. To achieve better controllability, the smallest valve (largest pressure drop) should be selected. With the valve outlet pressure much less than the inlet pressure, a large pressure drop results. There will now be an immediate reduction in capacity as the valve throttles. For steam valves, generally the largest possible pressure drop should be taken, without exceeding the critical pressure ratio. Therefore, the steam pressure drop should approach $80 \%$ of the system differential pressure.
Examining the pressure drops under "Recommended Pressure Drops for Valve Sizing - Steam", you might be concerned about the steam entering the coil at 0 psi when a large drop is taken across the control valve. Steam flow through the coil will still drop to vacuum pressures due to condensation of the steam. Consequently, a pressure differential will still exist. In this case, proper steam trapping and condensation piping is essential.


Figure 1.

## Recommended Pressure Drops for Valve Sizing Steam

1. With gravity flow condensate removal and inlet pressure less than 15 psi , use a pressure drop equal to the inlet gauge pressure.
2. With vacuum return system up to 7 CHg vacuum and an inlet pressure less than 2 psi , a pressure drop of 2 psi should be used. With an inlet pressure of 2 to 15 psi , use a pressure drop equal to the inlet gauge pressure.
3. With an inlet pressure greater than 15 psi , use a pressure drop equal to $80 \%$ of system differential pressure. Example: Inlet pressure is 20 psig ( 35 psia ) and a gravity return at atmospheric pressure 0 psig ( 14.7 psia ), use a pressure drop of 16 psi .
4. When a coil size is selected on the basis that line pressure and temperature is available in the coil of a heating and ventilating application, a very minimum pressure drop is desired. In this case, use the following: pressure drop:

| Initial Pressure | Pressure Drop |
| :---: | :---: |
| 15 psi | 5 psi |
| 50 psi | 7.5 psi |
| 100 psi | 10 psi |
| Over 100 psi | $10 \%$ of line pressure |

(typically on/off applications)

## The Most Important Variables to Consider

 When Sizing a Valve:1. What medium will the valve control? Water? Air? Steam? What effects will specific gravity and viscosity have on the valve size?
2. What will the inlet pressure be under maximum load demand? What is the inlet temperature?
3. What pressure drop (differential) will exist across the valve under maximum load demand?
4. What maximum capacity should the valve handle?
5. What is the maximum pressure differential the valve top must close against?
When these are known, a valve can be selected by formula (Cv method) or water and steam capacities tables which can be found in the Valves section, pages D-7 through D-10. The valve size should not exceed the line size.

## Valve Sizing and Selection Example

Select a valve to control a chilled water coil that must have a flow of 35 GPM with a valve differential pressure $(\triangle P)$ of 5 psi.
Determine the valve Cv using the formula for liquids.

$$
C v=Q \quad \sqrt{\frac{S}{P}}=35 G P M \sqrt{\frac{1}{5 p s i}}=15.6
$$

Select a valve that is suitable for this application and has a Cv as close as possible to the calculated value.

One choice is 277-03186: a 1-1/4" NC valve with a Cv of 16. Refer to Flowrite Valves Reference section.

## Valve Selection Criteria

1. Flow characteristic-Modified Equal Percentage which provides good control for a water coil.
2. Body rating and material-Suitable for water.
3. Valve type and action-A single seat NC valve with an adjustable spring range which can be sequenced with a NO valve used for heating.
4. Valve actuator-Actuator close-off rating is higher than the system differential pressure.
5. Valve line size—Its Cv is close to and slightly larger than the calculated Cv (15.6).
6. For Ball Valves-use the same selection criteria.

## Valve Body Rating

The temperature-pressure ratings for ANSI Classes 125 and 250 valve bodies made of bronze or cast iron are shown below.

| Description | Temperature | Pressure |  |
| :---: | :---: | :---: | :---: |
|  |  | ANSI Class 125 | ANSI Class 250 |
| Bronze Screwed Bodies <br> Specification \#B16.15-1978 <br> ANSI Amer. Std.; <br> USA; ASME | -20 to $+150^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+66^{\circ} \mathrm{C}\right)$ | $200 \mathrm{psi}(1378 \mathrm{kPa})$ | $400 \mathrm{psi}(2758 \mathrm{kPa})$ |
|  | -20 to $+200^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+93^{\circ} \mathrm{C}\right)$ | 190 psi ( 1310 kPa ) | 385 psi ( 2655 kPa ) |
|  | -20 to $+250^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+121^{\circ} \mathrm{C}\right)$ | 180 psi ( 1241 kPa ) | 365 psi ( 2586 kPa ) |
|  | -20 to $+300^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+149^{\circ} \mathrm{C}\right)$ | $165 \mathrm{psi}(1138 \mathrm{kPa})$ | $335 \mathrm{psi}(2300 \mathrm{kPa})$ |
|  | -20 to $+350^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+177^{\circ} \mathrm{C}\right)$ | 150 psi ( 1034 kPa ) | $300 \mathrm{psi}(2068 \mathrm{kPa})$ |
|  | -20 to $+400^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+204^{\circ} \mathrm{C}\right)$ | $125 \mathrm{psi}(862 \mathrm{kPa})$ | 250 psi (1724 kPa) |
| Cast Iron Flanged Bodies Class B-sizes 1 to 12 Specification \#B16.1 1975 ANSI Amer. Std.; USA; ASME | -20 to $+150^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+66^{\circ} \mathrm{C}\right)$ | 200 psi ( 1378 kPa ) | 500 psi (3445 kPa) |
|  | -20 to $+200^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+93^{\circ} \mathrm{C}\right)$ | 190 psi ( 1310 kPa ) | $460 \mathrm{psi}(3169 \mathrm{kPa})$ |
|  | -20 to $+225^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+106^{\circ} \mathrm{C}\right)$ | $180 \mathrm{psi}(1241 \mathrm{kPa})$ | $440 \mathrm{psi}(3032 \mathrm{kPa})$ |
|  | -20 to $+250^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+121^{\circ} \mathrm{C}\right)$ | 175 psi ( 1206 kPa ) | 415 psi ( 2859 kPa ) |
|  | -20 to $+275^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+135^{\circ} \mathrm{C}\right)$ | 170 psi ( 1171 kPa ) | 395 psi ( 2722 kPa ) |
|  | -20 to $+300^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+149^{\circ} \mathrm{C}\right)$ | 165 psi (1138 kPa) | 375 psi (2584 kPa) |
|  | -20 to $+325^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+163^{\circ} \mathrm{C}\right)$ | 155 psi (1069 kPa) | 355 psi ( 2448 kPa ) |
|  | -20 to $+350^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+177^{\circ} \mathrm{C}\right)$ | $150 \mathrm{psi}(1034 \mathrm{kPa})$ | 335 psi (2308 kPa) |
|  | -20 to $+375^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+191^{\circ} \mathrm{C}\right)$ | $145 \mathrm{psi}(1000 \mathrm{kPa})$ | $315 \mathrm{psi}(2170 \mathrm{kPa})$ |
|  | -20 to $+400^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+204^{\circ} \mathrm{C}\right)$ | $140 \mathrm{psi}(965 \mathrm{kPa})$ | 290 psi (1998 kPa) |
|  | -20 to $+425^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+218^{\circ} \mathrm{C}\right)$ | $130 \mathrm{psi}(896 \mathrm{kPa})$ | 270 psi ( 1860 kPa ) |
|  | -20 to $+450^{\circ} \mathrm{F}\left(-30\right.$ to $\left.+232^{\circ} \mathrm{C}\right)$ | $125 \mathrm{psi}(862 \mathrm{kPa})$ | 250 psi (1734 kPa) |

## SIEMENS

$\triangle \triangleleft$ 2-Way, Full-Port (no flow optimizer) Ball Valve Part Nos. and Flow Coefficients

| $$ |  | Valve <br> Part No. | Effective (Installed) Cv (Kvs) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Supply Line Size in Inches (mm) |
|  |  | $\begin{gathered} 1 / 2 \\ (13) \end{gathered}$ | $\begin{gathered} 3 / 4 \\ (20) \end{gathered}$ | $\begin{gathered} 1 \\ (25) \end{gathered}$ | $\begin{gathered} 1-1 / 4 \\ (32) \end{gathered}$ | $\begin{gathered} 1-1 / 2 \\ (38) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 2-1 / 2 \\ (63) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ |
| 1/2 | (15) |  | $\begin{aligned} & \text { 599-10307 or } \\ & \text { 599-10307S } \end{aligned}$ | $\begin{gathered} 10.0 \\ (8.62) \end{gathered}$ | $\begin{gathered} 6.94 \\ (5.93) \end{gathered}$ | $\begin{gathered} 6.19 \\ (5.29) \end{gathered}$ |  |  |  |  |  |
| $3 / 4$ | (20) |  | $\begin{aligned} & \text { 599-10311 or } \\ & \text { 599-10311S } \end{aligned}$ |  | $\begin{gathered} 25.00 \\ (21.55) \end{gathered}$ | $\begin{gathered} \hline 18.66 \\ (15.99) \end{gathered}$ | $\begin{gathered} 15.35 \\ (13.12) \end{gathered}$ |  |  |  |  |
| 1 | (25) | $\begin{aligned} & \text { 599-10316 or } \\ & \text { 599-10316S } \end{aligned}$ |  |  | $\begin{gathered} 63.00 \\ (54.31) \end{gathered}$ | $\begin{gathered} 39.78 \\ (34.00) \end{gathered}$ | $\begin{gathered} \hline 33.56 \\ (28.69) \end{gathered}$ |  |  |  |
| 1-1/4 | (30) | $\begin{aligned} & \text { 599-10321 or } \\ & 599-10321 \mathrm{~S} \end{aligned}$ |  |  |  | $\begin{aligned} & 100.00 \\ & (86.21) \end{aligned}$ | $\begin{aligned} & 69.19 \\ & (5.13) \end{aligned}$ | $\begin{gathered} \hline 51.45 \\ (43.98) \end{gathered}$ |  |  |
| 1-1/2 | (40) | $\begin{aligned} & \text { 599-10326 or } \\ & \text { 599-10326S } \end{aligned}$ |  |  |  |  | $\begin{gathered} 160.00 \\ (137.93) \end{gathered}$ | $\begin{gathered} 93.80 \\ (80.17) \end{gathered}$ | $\begin{gathered} 76.34 \\ (65.25) \end{gathered}$ |  |
| 2 | (50) | $\begin{aligned} & \text { 599-10329 or } \\ & \text { 599-10329S } \end{aligned}$ |  |  |  |  |  | $\begin{aligned} & 100.00 \\ & (86.21) \end{aligned}$ | $\begin{gathered} 94.30 \\ (80.60) \end{gathered}$ | $\begin{gathered} 86.12 \\ (73.61) \end{gathered}$ |

3-Way, Full-Port (no flow optimizer) Ball Valve Part Nos. and Flow Coefficients

| $\begin{gathered} \text { Valve } \\ \text { Size } \\ \text { in. }(\mathrm{mm}) \end{gathered}$ | Ball <br> Size <br> in. (mm) | Valve <br> Part No. | Effective (Installed) Cv (Kvs) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Supply Line Size in Inches (mm) |  |  |  |  |  |  |  |
|  |  |  | $\begin{gathered} 1 / 2 \\ (13) \end{gathered}$ | $\begin{gathered} 3 / 4 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 1 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 1-1 / 4 \\ (32) \end{gathered}$ | $\begin{gathered} 1-1 / 2 \\ (38) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \\ \hline \end{gathered}$ | $\begin{gathered} 2-1 / 2 \\ (63) \\ \hline \end{gathered}$ | $\begin{gathered} 3 \\ (76) \\ \hline \end{gathered}$ |
| 1/2 (15) | 3/4 (20) | 599-10255 | $\begin{gathered} 10.0 \\ (8.62) \end{gathered}$ | $\begin{gathered} 6.94 \\ (5.93) \end{gathered}$ | $\begin{gathered} 6.19 \\ (5.29) \end{gathered}$ |  |  |  |  |  |
| 3/4 (20) | 3/4 (20) | 599-10256 |  | $\begin{gathered} 16.00 \\ (13.79) \end{gathered}$ | 13.9 $(11.98)$ | $\begin{gathered} 12.4 \\ (10.69) \end{gathered}$ |  |  |  |  |
| 1 (25) | 1-1/4 (30) | 599-10259 |  |  | $\begin{gathered} 25.00 \\ (21.55) \end{gathered}$ | $\begin{gathered} 22.5 \\ (19.4) \end{gathered}$ | $\begin{gathered} 21.2 \\ (18.27) \end{gathered}$ |  |  |  |
| 1-1/4 (30) | 1-1/4 (30) | 599-10261 |  |  |  | $\begin{gathered} 40.00 \\ (34.48) \end{gathered}$ | $\begin{gathered} 36.9 \\ (31.81) \end{gathered}$ | $\begin{gathered} 33.3 \\ (28.70) \end{gathered}$ |  |  |
| 1-1/2 (40) | 1-1/2 (40) | 599-10264 |  |  |  |  | $\begin{gathered} 63.00 \\ (54.31) \end{gathered}$ | $\begin{gathered} 55.3 \\ (47.67) \end{gathered}$ | $\begin{gathered} 51.00 \\ (43.96) \end{gathered}$ |  |
| 2 (50) | 2 (50) | 599-10267 |  |  |  |  |  | $\begin{gathered} 100 \\ (86.21) \end{gathered}$ | $\begin{gathered} 94.3 \\ (81.29) \end{gathered}$ | 86.1 $(74.23)$ |

Key Valve may be oversizedOptimal valve size
Valve may be undersized

## Valve Sizing Formulas

The following definitions apply in the following formulas:

| Cv | Valve flow coefficient, U.S. GPM with $\mathrm{P}=1 \mathrm{psi}$ |
| :---: | :---: |
| $\mathrm{P}_{1}$ | Inlet pressure at maximum flow, psia (abs.) |
| $\mathrm{P}_{2}$ | Outlet pressure at maximum flow, psia (abs.) |
| $\triangle \mathrm{P}$ | $\mathrm{P}_{1}-\mathrm{P}_{2}$ at maximum flow, psi |
| Q | Fluid flow, U.S. GPM |
| Qa | Air or gas flow, standard cubic feet per hour (SCFH) at 14.7 psi and $60^{\circ} \mathrm{F}$ |
| W | Steam flow, pounds per hour (lb./hr.) |
| S | Specific gravity of fluid relative to water @ $60^{\circ} \mathrm{F}$ |
| G | Specific gravity of gas relative to air at 14.7 psi and $60^{\circ} \mathrm{F}$ |
| T | Flowing air or gas temperature ( ${ }^{\circ} \mathrm{F}$ ) |
| K | $1+\left(0.0007 \mathrm{x}^{\circ} \mathrm{F}\right.$ superheat), for steam |
| $\mathrm{V}_{2}$ | Specific volume, cubic feet per pound, at outlet pressure $\mathrm{P}_{2}$ and absolute temperature ( $\mathrm{T}+460$ ) |
| $\mathrm{K}_{\mathrm{r}}$ | Viscosity correction factor for fluids (See Page I-4) |


| Formulas: | Remarks: |
| :---: | :---: |
| 1. For liquids (water, oil, etc.): $\mathrm{Cv}=\mathrm{Q} \quad \sqrt{\frac{\mathrm{~S}}{\triangle \mathrm{P}}}$ $C v=K_{r} Q \sqrt{\frac{S}{\triangle P}}$ | Specific gravity correction is negligible for water below $200^{\circ} \mathrm{F}$ (use $\mathrm{S}=1.0$ ). Use actual specific gravity $S$ of other liquids at actual flow temperature. <br> Use this for fluids with viscosity correction fact. Use actual specific gravity $S$ for fluids at actual flow temperature. |
| 2. For gases (air, natural gas, propane, etc.): $\begin{aligned} & C v=\frac{Q a \sqrt{G(T+460})}{1360 \sqrt{\triangle P\left(P_{2}\right)}}- \\ & C v=\frac{Q a \sqrt{G(T+460)}}{660 P_{1}} \end{aligned}$ | Use this when $P_{2}$ is greater than $1 / 2 \mathrm{P}_{1}$. <br> Use this when $P_{2}$ is less than or equal to $1 / 2 \mathrm{P}_{1}$. |
| 3. For steam (saturated or superheated): $\begin{aligned} & C v=\frac{W K}{2.1 \sqrt{\triangle P\left(P_{1}+P_{2}\right)}} \\ & C v=\frac{W K}{1.82 P_{1}} \end{aligned}$ | Use this when $P_{2}$ is greater than $1 / 2 P_{1}$. <br> Use this when P 2 is less than or equal to $1 / 2 \mathrm{P}_{1}$. |
| 4. For vapors other than steam: $C v=\frac{W K}{63.4} \sqrt{\frac{V_{2}}{\triangle P}}$ | When $P_{2}$ is less than or equal to $1 / 2 P_{1}$, use the value of $1 / 2 P_{1}$ in place of $P$ and use $P_{2}$ corresponding to $1 / 2 P_{1}$ when determining specific volume $V_{2}$. |

## Viscosity Factors

The relationship between kinematic and absolute viscosity:
Centistoke =
Centipoise
Specific Gravity

| Saybolt* Univ Seconds (S.S.U.) | Engler Time Seconds | Kinematic Viscosity | Correction Factors |
| :---: | :---: | :---: | :---: |
| 46,350 | - | 10,000 | - |
| 37,080 | - | 8,000 | - |
| 27,810 | - | 6,000 | - |
| 18,540 | - | 4,000 | - |
| 13,900 | - | 3,000 | - |
| 11,590 | - | 2,500 | - |
| 9,270 | - | 2,000 | 1.93 |
| 6,950 | 10,800 | 1,500 | 1.90 |
| 4,635 | 7,100 | 1,000 | 1.82 |
| 3,708 | 5,700 | 800 | 1.78 |
| 2,781 | 4,250 | 600 | 1.74 |
| 1,854 | 2,820 | 400 | 1.67 |
| 1,390 | 2,120 | 300 | 1.63 |
| 1,159 | 1,760 | 250 | 1.61 |
| 927 | 1,400 | 200 | 1.57 |
| 695 | 1,050 | 150 | 1.43 |
| 464 | 700 | 100 | 1.45 |
| 371 | 555 | 80 | 1.42 |
| 278 | 420 | 60 | 1.37 |
| 186 | 290 | 40 | 1.30 |
| 141 | 225 | 30 | 1.25 |
| 119 | 191 | 25 | 1.22 |
| 97.8 | 157 | 20 | 120 |
| 77.4 | 127 | 15 | 1.16 |
| 58.9 | 97 | 10 | 1.11 |
| 52.1 | 85.5 | 8 | 1.08 |
| 45.6 | 76.0 | 6 | 1.07 |
| 39.1 | 67.5 | 4 | 1.05 |
| 36.0 | 62.5 | 3 | 1.03 |
| 32.6 | 58.0 | 2 | - |
| 31.6 | 55.5 | 1.5 | - |
| $31.3 \leftarrow$ PURE WATER AT $60^{\circ} \mathrm{F} \rightarrow 1.1$ |  |  | - |

Chart Note
*Redwood time (seconds) approximately same as S.S.U.

## Specific Gravity of Water

| Temp <br> $\mathbf{T}\left({ }^{\circ} \mathrm{F}\right)$ | Abs. <br> Pressure | Specific Gravity - S <br> $\left(\mathbf{W}=62.4 \mathrm{lb} . / \mathrm{ft} .^{3} @\right.$ 60 $\left.{ }^{\circ} \mathrm{F}\right)$ | $\sqrt{\mathrm{S}}$ |
| :---: | :---: | :---: | :---: |
| 60 | - | 1.000 | 1.000 |
| 100 | - | 0.993 | 0.999 |
| 150 | - | 0.981 | 0.985 |
| 200 | - | 0.963 | 0.981 |
| 250 | 30 | 0.942 | 0.971 |
| 300 | 67 | 0.920 | 0.959 |
| 350 | 135 | 0.891 | 0.944 |
| 400 | 247 | 0.860 | 0.927 |
| 450 | 423 | 0.827 | 0.910 |

## Sizing Formulas and Tables

## Process Formulas

For Heating or Cooling Water:
GPM =
Btu/hr.
( ${ }^{\circ}$ F water temp. rise or drop $\times 500$ )
GPM = $\qquad$
${ }^{\circ} \mathrm{F}$ water temperature change
( $\mathrm{H}=$ change in enthalpy of air expressed in Btu/lb. of air)
For Heating Water with Steam:
lbs. steam $/ \mathrm{hr}$. $=0.50 \times$ GPM $\times\left({ }^{\circ} \mathrm{F}\right.$ water temp. rise $)$
For Heating or Cooling Water:
$\mathrm{GPM}_{1}=\mathrm{GPM}_{2} \times \quad\left({ }^{\circ} \mathrm{F}\right.$ water ${ }_{2}$ temp. rise or drop)
${ }^{\circ} \mathrm{F}$ water ${ }_{1}$ temp. drop
For Heating Air with Steam Coils:
lbs. steam $/ \mathrm{hr}$. $=1.08 \times\left({ }^{\circ} \mathrm{F}\right.$ air temp. rise $) \times \mathrm{CFM}$
1000
For Heating Air with Water Coils:
GPM $=2.16 \times \frac{\mathrm{CFM} \times\left({ }^{\circ} \mathrm{F} \text { air temp. rise }\right)}{1000 \times\left({ }^{\circ} \mathrm{F} \text { water }{ }_{1} \text { temp. drop }\right)}$

## For Radiation:

lbs. steam/hr. $=0.24 \times \mathrm{ft} .^{2}$ EDR (Low pressure steam)
EDR = Equivalent Direct Radiation
1 EDR (steam) $=240$ BTU/Hr. (Coil Temp. $=215^{\circ} \mathrm{F}$ )
1 EDR (water) $=200 \mathrm{BTU} / \mathrm{Hr}$. (Coil Temp. $=197^{\circ} \mathrm{F}$ )
$\mathrm{GPM}=\frac{\mathrm{ft} .{ }^{2} \mathrm{EDR}}{50}$
(Assume $20^{\circ} \mathrm{F}$ water TD)

## MZ Series

| Valve Size | 2-way | 3-way |
| :---: | :---: | :---: |
|  | Electronic |  |
| Normally Open |  |  |
| 1/2", Cv $\leq 1.6$ | $60 \mathrm{psi}(414 \mathrm{kPa})$ | $25 \mathrm{psi}(172 \mathrm{kPa})$ |
| $1 / 2$ ", Cv $\leq 4$ | $35 \mathrm{psi}(241 \mathrm{kPa})$ | $15 \mathrm{psi}(103 \mathrm{kPa})$ |
| $3 / 4$ to 1 ", $\mathrm{Cv} \leq 10$ | $30 \mathrm{psi}(207 \mathrm{kPa})$ | $10 \mathrm{psi}(69 \mathrm{kPa})$ |
| Normally Closed |  |  |
| 1/2", Cv $\leq 1.6$ | $70 \mathrm{psi}(482 \mathrm{kPa})$ | $70 \mathrm{psi}(482 \mathrm{kPa})$ |
| 1/2", Cv $\leq 4$ | $40 \mathrm{psi}(276 \mathrm{kPa})$ | $40 \mathrm{psi}(276 \mathrm{kPa})$ |
| $3 / 4$ to 1 " $\mathrm{Cv} \leq 10$ | $30 \mathrm{psi}(207 \mathrm{kPa})$ | $30 \mathrm{psi}(207 \mathrm{kPa})$ |

Table Note: For 3-way valve close-offs, use this chart to determine upper port (NC) and bottom port (NO).

## MT Series

| 2-Way Valve Size | Pneumatic |  |  | Electronic |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 599-01088 |  |  | SQS | SSC |
|  | 3-8 psi | 8-13 psi | 10-15 psi |  |  |
|  | Normally Open |  |  |  |  |
| 1/2", Cv $\leq 1.6$ | 95 psi (655 kPa) | $45 \mathrm{psi}(310 \mathrm{kPa})$ | $20 \mathrm{psi}(138 \mathrm{kPa})$ | 160 psi (1103 kPa) | 120 psi (868 kPa) |
| 1/2", Cv $\leq 4$ | $45 \mathrm{psi}(310 \mathrm{kPa})$ | $25 \mathrm{psi}(172 \mathrm{kPa})$ | $15 \mathrm{psi}(103 \mathrm{kPa})$ | $85 \mathrm{psi}(586 \mathrm{kPa})$ | $65 \mathrm{psi}(448 \mathrm{kPa})$ |
| $3 / 4$ to 1 ', Cv $\leq 10$ | 35 psi (241 kPa) | $10 \mathrm{psi}(69 \mathrm{kPa})$ | - | $70 \mathrm{psi}(482 \mathrm{kPa})$ | $55 \mathrm{psi}(379 \mathrm{kPa})$ |
|  | Normally Closed |  |  |  |  |
| 1/2", Cv $\leq 1.6$ | 40 psi (276 kPa) | $95 \mathrm{psi}(655 \mathrm{kPa})$ | $95 \mathrm{psi}(655 \mathrm{kPa})$ | 95 psi (655 kPa) | 95 psi (655 kPa) |
| 1/2", Cv $\leq 4$ | 28 psi (193 kPa) | $50 \mathrm{psi}(345 \mathrm{kPa})$ | $50 \mathrm{psi}(345 \mathrm{kPa})$ | $50 \mathrm{psi}(345 \mathrm{kPa})$ | $50 \mathrm{psi}(345 \mathrm{kPa})$ |
| $3 / 4$ to 1 ', Cv $\leq 10$ | 18 psi (124 kPa) | $40 \mathrm{psi}(276 \mathrm{kPa})$ | 40 psi (276 kPa) | $40 \mathrm{psi}(276 \mathrm{kPa})$ | 40 psi (276 kPa) |


| 3-Way Valve Size | Pneumatic |  |  | Electronic |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 599-01088 |  |  | SQS | SSC |
|  | 3-8 psi | 8-13 psi | 10-15 psi |  |  |
|  | Normally Open |  |  |  |  |
| 1/2", Cv $\leq 1.6$ | 95 psi (655 kPa) | $45 \mathrm{psi}(310 \mathrm{kPa})$ | 20 psi (138 kPa) | 160 psi (1103 kPa) | $95 \mathrm{psi}(655 \mathrm{kPa})$ |
| 1/2", Cv $\leq 4$ | $45 \mathrm{psi}(310 \mathrm{kPa})$ | $25 \mathrm{psi}(172 \mathrm{kPa})$ | 15 psi (103 kPa) | $85 \mathrm{psi}(586 \mathrm{kPa})$ | $50 \mathrm{psi}(379 \mathrm{kPa})$ |
| $3 / 4$ to 1 ', $\mathrm{Cv} \leq 10$ | $35 \mathrm{psi}(241 \mathrm{kPa})$ | $10 \mathrm{psi}(69 \mathrm{kPa})$ | - | $70 \mathrm{psi}(482 \mathrm{kPa})$ | 40 psi (276 kPa) |
|  | Normally Closed |  |  |  |  |
| 1/2", Cv $\leq 1.6$ | 40 psi (276 kPa) | $95 \mathrm{psi}(655 \mathrm{kPa})$ | $120 \mathrm{psi}(827 \mathrm{kPa})$ | $95 \mathrm{psi}(655 \mathrm{kPa})$ | $95 \mathrm{psi}(655 \mathrm{kPa})$ |
| 1/2", Cv $\leq 4$ | $28 \mathrm{psi}(193 \mathrm{kPa})$ | $50 \mathrm{psi}(345 \mathrm{kPa})$ | $65 \mathrm{psi}(448 \mathrm{kPa})$ | $50 \mathrm{psi}(345 \mathrm{kPa})$ | $50 \mathrm{psi}(345 \mathrm{kPa})$ |
| $3 / 4$ to 1 ", $\mathrm{Cv} \leq 10$ | $18 \mathrm{psi}(124 \mathrm{kPa})$ | $40 \mathrm{psi}(276 \mathrm{kPa})$ | $50 \mathrm{psi}(345 \mathrm{kPa})$ | $40 \mathrm{psi}(276 \mathrm{kPa})$ | $40 \mathrm{psi}(276 \mathrm{kPa})$ |

Table Notes:
For 3-Way valve close-offs, use this chart to determine upper (NC) and bottom port (NO).
Normally open close-off pressures are at 20 psi actuator pressure.
Normally closed close-off pressures are at 0 psi actuator pressure.

## SIEMENS

| 2-Way Valve Body Part No. | Valve Size in. | Flow Rate Cv | Close Off psi |
| :---: | :---: | :---: | :---: |
| 599-10300 / 599-10300S |  | 0.4 | 200 |
| 599-10301/ 599-10301S |  | 0.63 | 200 |
| 599-10302 / 599-10302S |  | 1.0 | 200 |
| 599-10303 / 599-10303S | $1 / 2$ | 1.6 | 200 |
| 599-10304 / 599-10304S | $1 / 2$ | 2.5 | 200 |
| 599-10305 / 599-10305S |  | 4.0 | 200 |
| 599-10306 / 599-10306S |  | 6.3 | 200 |
| 599-10307* 599-10307S* |  | 10 | 200 |
| 599-10308 / 599-10308S |  | 6.3 | 200 |
| 599-10309 / 599-10309S | 314 | 10 | 200 |
| 599-10310 / 599-10310S | $3 / 4$ | 16 | 200 |
| 599-10311*/599-10311S* |  | 25 | 200 |
| 599-10312 / 599-10312S |  | 10 | 200 |
| 599-10313 / 599-10313S |  | 16 | 200 |
| 599-10314 / 599-10314S | 1 | 25 | 200 |
| 599-10315 / 599-10315S |  | 40 | 200 |
| 599-10316*/599-10316S* |  | 63 | 200 |
| 599-10317 / 599-10317S |  | 16 | 200 |
| 599-10318 / 599-10318S |  | 25 | 200 |
| 599-10319 / 599-10319S | 1-1/4 | 40 | 200 |
| 599-10320 / 599-10320S |  | 63 | 200 |
| 599-10321* 599-10321S* |  | 100 | 200 |
| 599-10322 / 599-10322S |  | 25 | 200 |
| 599-10323 / 599-10323S |  | 40 | 200 |
| 599-10324 / 599-10324S | 1-1/2 | 63 | 200 |
| 599-10325/599-10325S |  | 100 | 200 |
| 599-10326*/599-10326S* |  | 160 | 200 |
| 599-10327 / 599-10327S |  | 40 | 200 |
| 599-10328 / 599-10328S | 2 | 63 | 200 |
| 599-10329*/ 599-10329S* | 2 | 100 | 200 |
| 599-10330 / 599-10330S |  | 160 | 200 |


| 3-Way Valve Body Part No. | Valve Size in. | Flow Rate Cv | Close Off psi |
| :---: | :---: | :---: | :---: |
| 599-10250 | 1/2 | 0.4 | 50 |
| 599-10251 |  | 0.63 | 50 |
| 599-10252 |  | 1.0 | 50 |
| 599-10253 |  | 2.5 | 50 |
| 599-10254 |  | 4.0 | 50 |
| 599-10255 |  | 10 | 50 |
| 599-10256 | 3/4 | 16 | 50 |
| 599-10257 | 1 | 10 | 50 |
| 599-10258 |  | 16 | 50 |
| 599-10259* |  | 25 | 50 |
| 599-10260 | 1-1/4 | 16 | 40 |
| 599-10261 |  | 40 | 40 |
| 599-10262 | 1-1/2 | 16 | 40 |
| 599-10263 |  | 25 | 40 |
| 599-10264* |  | 63 | 40 |
| 599-10265 | 2 | 25 | 40 |
| 599-10266* |  | 40 | 40 |
| 599-10267 |  | 100 | 40 |

* Denotes a full-port valve with no flow optimizer insert.
* Denotes a full-port valve with no flow optimizer insert.


## Electronic

| $$ |  | $\begin{aligned} & \text { SAX SR } \\ & \text { APC } \\ & 370 / 372 \end{aligned}$ | $\begin{aligned} & \text { SAX NSR } \\ & \text { APC } \\ & 371 / 373 \end{aligned}$ | $\begin{gathered} \text { SKD } \\ \text { APC } \\ 274-276 \end{gathered}$ | $\begin{gathered} \text { SKB } \\ \text { APC } \\ 289-291 \end{gathered}$ | $\begin{gathered} \text { SKC } \\ \text { APC } \\ 292-294 \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Normally Open |  |  |  |  |  |  |
| 1/2 | (15) | 250 (1724) | 250 (1724) | 250 (1724) | 250 (1724) | - |
| 3/4 | (20) | 182 (1255) | 211 (1456) | 250 (1724) | 250 (1724) | - |
| 1 | (25) | 119 (821) | 137 (945) | 201 (1386) | 250 (1724) | - |
| 1-1/4 | (32) | 73 (503) | 85 (586) | 124 (855) | 250 (1724) | - |
| 1-1/2 | (40) | 47 (324) | 55 (379) | 80 (552) | 250 (1724) | - |
| 2 | (50) | 29 (200) | 34 (235) | 49 (338) | 201 (1386) | - |
| 2-1/2 | (65) | 23 (159) | 26 (179) | 38 (262) | 153 (518) | - |
| 3 | (80) | 15 (103) | 17 (117) | 25 (172) | 101 (342) | - |
| 4 | (100) | - | - | - | - | 65 (448) |
| 5 | (125) | - | - | - | - | 42 (289) |
| 6 | (150) | - | - | - | - | 29 (199) |
| Normally Closed |  |  |  |  |  |  |
| 1/2 | (15) | 250 (1724) | 250 (1724) | 250 (1724) | 250 (1724) | - |
| 3/4 | (20) | 234 (1614) | 250 (1724) | 250 (1724) | 250 (1724) | - |
| 1 | (25) | 137 (945) | 159 (1097) | 203 (1400) | 250 (1724) | - |
| 1-1/4 | (32) | 80 (552) | 92 (634) | 117 (807) | 250 (1724) | - |
| 1-1/2 | (40) | 50 (345) | 57 (393) | 73 (503) | 208 (1434) | - |
| 2 | (50) | 30 (207) | 35 (241) | 44 (303) | 126 (869) | - |
| 2-1/2 | (65) | 23 (159) | 26 (179) | 34 (234) | 97 (668) | - |
| 3 | (80) | 15 (103) | 17 (117) | 22 (152) | 63 (434) | - |
| 4 | (100) | - | - | - | - | 39 (268) |
| 5 | (125) | - | - | - | - | 25 (172) |
| 6 | (150) | - | - | - | - | 17 (117) |

## Electronic High Pressure Close-off

| $\begin{aligned} & \text { Valve Size } \\ & \text { in. } \quad(\mathrm{mm}) \end{aligned}$ |  | Electro-Hydraulic 24 VAC |  |
| :---: | :---: | :---: | :---: |
|  |  | SKD | SKC |
|  |  | Normally Open |  |
| 2-1/2 | (65) | 200 (1378) | - |
| 3 | (80) | 200 (1378) | - |
| 4 | (100) | - | 200 (1378) |
| 5 | (125) | - | 200 (1378) |
| 6 | (150) | - | 200 (1378) |
|  |  | Normally Closed |  |
| 2-1/2 | (65) | 200 (1378) | - |
| 3 | (80) | 200 (1378) | - |
| 4 | (100) | - | 200 (1378) |
| 5 | (125) | - | 200 (1378) |
| 6 | (150) | - | 200 (1378) |

Table Notes:
All values within table are in psi ( kPa ) unless otherwise indicated..

## SIEMENS

Pneumatic

| Valve Size in. (mm) | Spring Range |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 to $8 \mathrm{psi}(21$ to 55 kPa$)$ |  |  |  |  | 10 to 15 psi ( 69 to 103 kPa ) |  |  |
|  | 4" Actuator | 8" Actuator |  | 12" Actuator |  | 4" Actuator | 8" Actuator | 12" Actuator |
|  | $\begin{gathered} 15 \mathrm{psi} \\ (103 \mathrm{kPa}) \end{gathered}$ | $\begin{gathered} 15 \mathrm{psi} \\ (103 \mathrm{kPa}) \end{gathered}$ | $\begin{gathered} 30 \mathrm{psi} \\ (207 \mathrm{kPa}) \end{gathered}$ | $\begin{gathered} 15 \mathrm{psi} \\ (103 \mathrm{kPa}) \end{gathered}$ | $\begin{gathered} 30 \mathrm{psi} \\ (207 \mathrm{kPa}) \end{gathered}$ | $\begin{gathered} 0 \mathrm{psi} \\ (0 \mathrm{kPa}) \end{gathered}$ | $\begin{gathered} 0 \mathrm{psi} \\ (0 \mathrm{kPa}) \end{gathered}$ | $\begin{gathered} 0 \mathrm{psi} \\ (0 \mathrm{kPa}) \end{gathered}$ |
|  | Normally Open |  |  |  |  | Normally Closed |  |  |
| 1/2 (15) | 142 (979) | 250 (1724) | 250 (1724) | - | - | 236 (1627) | 250 (1724) | - |
| 3/4 (20) | 80 (552) | 231 (1593) | 250 (1724) | - | - | 155 (1069) | 250 (1724) | - |
| 1 (25) | 52 (359) | 150 (1034) | 250 (1724) | 250 (1724) | 250 (1724) | 91 (627) | 250 (1724) | 250 (1724) |
| 1-1/4 (32) | 32 (221) | 93 (641) | 250 (1724) | 250 (1724) | 250 (1724) | 52 (359) | 148 (1020) | 250 (1724) |
| 1-1/2 (40) | 20 (138) | 60 (414) | 198 (1365) | 205 (1413) | 250 (1724) | 32 (331) | 92 (634) | 250 (1724) |
| 2 (50) | 12 (83) | 37 (255) | 123 (848) | 130 (896) | 250 (1724) | 20 (138) | 55 (379) | 185 (1275) |
| 2-1/2 (65) | - | 31 (213) | 100 (689) | 95 (655) | 250 (1724) | - | 36 (248) | 114 (786) |
| 3 (80) | - | 20 (138) | 66 (444) | 63 (434) | 200 (1378) | - | 23 (158) | 74 (610) |
| 4 (100) | - | - | - | 40 (275) | 129 (889) | - | - | 46 (317) |
| 5 (125) | - | - | - | 26 (179) | 82 (565) | - | - | 29 (199) |
| 6 (150) | - | - | - | 18 (124) | 57 (393) | - | - | 20 (137) |

Table Notes:
All values within table are in psi $(\mathrm{kPa})$ unless otherwise indicated.
For 3-Way valve close-offs, use this chart to determine upper port (NC) and bottom port (NO).
Normally open close-off pressures are at 15 psi actuator pressure.
Normally closed close-off pressures are at 0 psi actuator pressure.

## Pneumatic High Pressure Close-off

| Valve Size <br> in. (mm) | Spring Range |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 3 to 8 psi (21 to 55 kPa ) |  | 10 to 15 psi ( 69 to 103 kPa ) |  |
|  | 8" Actuator | 12" Actuator | 8" Actuator | 12" Actuator |
|  | Normally Open |  | Normally Closed |  |
| 2-1/2 (65) | 200 (1378) | - | 200 (1378) | - |
| 3 (80) | 200 (1378) | - | 200 (1378) | - |
| 4 (100) | - | 200 (1378) | - | 200 (1378) |
| 5 (125) | - | 200 (1378) | - | 200 (1378) |
| 6 (150) | - | 200 (1378) | - | 200 (1378) |

Table Notes:
All values within table are in psi (kPa) unless otherwise indicated.

## 2-1/2 to 8-inch Cast Iron Flange Dimensions (as defined by ANSI standard B16.1)



ANSI Class 125

| Nominal Pipe Size | Flanges |  | Drilling |  | Bolting |  | Length of Machine Bolts F |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Flange Diameter | Flange Thickness | Diameter of Bolt Circle | Diameter of Bolt Holes | Number of Bolts | Diameter of Bolts |  |
|  | A | B | D | E |  |  |  |
| 2-1/2" | $7{ }^{\text {7 }}$ | 11/16" | 5-1/2" | $3 / 4$ " | 4 | 5/8" | 2-1/2" |
| 3" | 7-1/2" | 3/4" | $6 "$ | $3 / 4 "$ | 4 | 5/8" | 2-1/2" |
| 4" | $9{ }^{9}$ | 15/16" | 7-1/2" | $3 / 4 "$ | 8 | 5/8" | 3" |
| 5" | 10" | 15/16" | 8-1/2" | 7/8" | 8 | $3 / 4 "$ | 3" |
| $6 "$ | 11 | $1{ }^{\prime \prime}$ | 9-1/2" | 7/8" | 8 | 3/4" | 3-1/4" |
| 8" | 13-1/2" | 1-1/8" | 11-3/4" | 7/8" | 8 | 7/8" | 3-1/2" |

ANSI Class 250

| Nominal Pipe Size | Flanges |  |  | Drilling |  | Bolting |  | Length of Machine Bolts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Flange Diameter | Flange Thickness | Diameter of Raised Face | Diameter of Bolt Circle | Diameter of Bolt Holes | Number of Bolts | Diameter of Bolts |  |
|  | A | B | C | D | E |  |  | F |
| 2-1/2" | 7-1/2" | $1 "$ | 4-15/16" | 5-7/8" | 7/8" | 8 | 3/4" | 3-1/4" |
| 3" | 8-1/4" | 1-1/8" | 5-11/16" | 6-5/8" | 7/8" | 8 | 3/4" | 3-1/5" |
| $4 "$ | 10" | 1-1/4" | 6-15/16" | 7-7/8" | 7/8" | 8 | 3/4" | 3-3/4" |
| 5" | 11" | 1-3/8" | 8-5/16" | 9-1/4" | 7/8" | 8 | 3/4" | 4" |
| $6 "$ | 12-1/2" | 1-7/16" | 9-11/16" | 10-5/8" | 7/8" | 12 | 3/4" | 4" |
| 8" | 15 " | 1-5/8" | 11-15/16" | $13 "$ | $1 "$ | 12 | 7/8" | 4-1/2" |

## SIEMENS

| Vacuum <br> Inches <br> Hg | Absolute <br> Pressure <br> psi | Temperature <br> degrees <br> Fahrenheit |
| :---: | :---: | :---: |
| 29.74 | 0.0886 | 32 |
| 29.67 | 0.1217 | 40 |
| 29.56 | 0.1780 | 50 |
| 29.40 | 0.2562 | 60 |
| 29.18 | 0.3626 | 70 |
| 28.89 | 0.505 | 80 |
| 28.50 | 0.696 | 90 |
| 28.00 | 0.946 | 100.00 |
| 27.88 | 1 | 101.83 |
| 25.85 | 2 | 126.15 |
| 23.81 | 3 | 141.52 |
| 21.78 | 4 | 153.01 |
| 19.74 | 5 | 162.28 |
| 17.70 | 6 | 170.06 |
| 15.67 | 7 | 176.85 |
| 13.63 | 8 | 182.86 |
| 11.60 | 9 | 188.27 |
| 9.56 | 10 | 193.22 |
| 7.52 | 11 | 197.75 |
| 5.49 | 12 | 201.96 |
| 3.45 | 13 | 205.87 |
| 1.42 | 14 | 209.55 |


| Gauge Pressure psi | Absolute Pressure psi | Temperature degrees Fahrenheit |
| :---: | :---: | :---: |
| 0.0 | 14.70 | 212.0 |
| 0.3 | 15 | 213.0 |
| 1.3 | 16 | 216.3 |
| 2.3 | 17 | 219.4 |
| 3.3 | 18 | 222.4 |
| 4.3 | 19 | 225.2 |
| 5.3 | 20 | 228.0 |
| 6.3 | 21 | 230.6 |
| 7.3 | 22 | 233.1 |
| 8.3 | 23 | 235.5 |
| 9.3 | 24 | 237.8 |
| 10.3 | 25 | 240.1 |
| 11.3 | 26 | 242.2 |
| 12.3 | 27 | 244.4 |
| 13.3 | 28 | 246.4 |
| 14.3 | 29 | 248.4 |
| 15.3 | 30 | 250.3 |
| 16.3 | 31 | 252.2 |
| 17.3 | 32 | 254.1 |
| 18.3 | 33 | 255.8 |
| 19.3 | 34 | 257.6 |
| 20.3 | 35 | 259.3 |
| 21.3 | 36 | 261.0 |
| 22.3 | 37 | 262.6 |
| 23.3 | 38 | 264.2 |
| 24.3 | 39 | 265.8 |
| 25.3 | 40 | 267.3 |
| 26.3 | 41 | 268.7 |
| 27.3 | 42 | 270.2 |
| 28.3 | 43 | 271.7 |
| 29.3 | 44 | 273.1 |


| Gauge Pressure psi | Absolute Pressure psi | Temperature degrees <br> Fahrenheit |
| :---: | :---: | :---: |
| 30.3 | 45 | 274.5 |
| 31.3 | 46 | 275.8 |
| 32.3 | 47 | 277.2 |
| 33.3 | 48 | 278.5 |
| 34.3 | 49 | 279.8 |
| 35.3 | 50 | 281.0 |
| 36.3 | 51 | 282.3 |
| 37.3 | 52 | 283.5 |
| 38.3 | 53 | 284.7 |
| 39.3 | 54 | 285.9 |
| 40.3 | 55 | 287.1 |
| 41.3 | 56 | 288.2 |
| 42.3 | 57 | 289.4 |
| 43.3 | 58 | 290.5 |
| 44.3 | 59 | 291.6 |
| 45.3 | 60 | 292.7 |
| 46.3 | 61 | 293.8 |
| 47.3 | 62 | 294.9 |
| 48.3 | 63 | 295.9 |
| 49.3 | 64 | 297.0 |
| 50.3 | 65 | 298.0 |
| 51.3 | 66 | 299.0 |
| 52.3 | 67 | 300.0 |
| 53.3 | 68 | 301.0 |
| 54.3 | 69 | 302.0 |
| 55.3 | 70 | 302.9 |
| 56.3 | 71 | 303.9 |
| 57.3 | 72 | 304.8 |
| 58.3 | 73 | 305.8 |
| 59.3 | 74 | 306.7 |
| 60.3 | 75 | 307.6 |
| 61.3 | 76 | 308.5 |
| 62.3 | 77 | 309.4 |
| 63.3 | 78 | 310.3 |
| 64.3 | 79 | 311.2 |
| 65.3 | 80 | 312.0 |
| 66.3 | 81 | 312.9 |
| 67.3 | 82 | 313.8 |
| 68.3 | 83 | 314.6 |
| 69.3 | 84 | 315.4 |
| 70.3 | 85 | 316.3 |
| 71.6 | 86 | 317.1 |
| 72.3 | 87 | 317.9 |
| 73.3 | 88 | 318.7 |
| 74.3 | 89 | 319.5 |
| 75.3 | 90 | 320.3 |
| 76.3 | 91 | 321.1 |
| 77.3 | 92 | 321.8 |
| 78.3 | 93 | 322.6 |
| 79.3 | 94 | 323.4 |
| 80.3 | 95 | 324.1 |
| 81.3 | 96 | 324.9 |
| 82.3 | 97 | 325.6 |
| 83.3 | 98 | 326.4 |
| 84.3 | 99 | 327.1 |
| 85.3 | 100 | 327.8 |
| 87.3 | 102 | 329.3 |
| 89.3 | 104 | 330.7 |
| 91.3 | 106 | 332.0 |
| 93.3 | 108 | 333.4 |
| 95.3 | 110 | 334.8 |


| Gauge Pressure psi | Absolute Pressure psi | Temperature degrees <br> Fahrenheit |
| :---: | :---: | :---: |
| 97.3 | 112 | 336.1 |
| 99.3 | 114 | 337.4 |
| 101.3 | 116 | 338.7 |
| 103.3 | 118 | 340.0 |
| 105.3 | 120 | 341.3 |
| 107.3 | 122 | 342.5 |
| 109.3 | 124 | 343.8 |
| 111.3 | 126 | 345.0 |
| 113.3 | 128 | 346.2 |
| 115.3 | 130 | 347.4 |
| 117.3 | 132 | 348.5 |
| 119.3 | 134 | 349.7 |
| 121.3 | 136 | 350.8 |
| 123.3 | 138 | 352.0 |
| 125.3 | 140 | 353.1 |
| 127.3 | 142 | 354.2 |
| 129.3 | 144 | 355.3 |
| 131.3 | 146 | 356.3 |
| 133.3 | 148 | 357.4 |
| 135.3 | 150 | 358.5 |
| 137.3 | 152 | 359.5 |
| 139.3 | 154 | 360.5 |
| 141.3 | 156 | 361.6 |
| 143.3 | 158 | 362.6 |
| 145.3 | 160 | 363.6 |
| 147.3 | 162 | 364.6 |
| 149.3 | 164 | 365.6 |
| 151.3 | 166 | 366.5 |
| 153.3 | 168 | 367.5 |
| 155.3 | 170 | 368.5 |
| 157.3 | 172 | 369.4 |
| 159.3 | 174 | 370.4 |
| 161.3 | 175 | 371.3 |
| 163.3 | 178 | 372.2 |
| 165.3 | 180 | 373.1 |
| 167.3 | 182 | 374.0 |
| 169.3 | 184 | 374.9 |
| 171.3 | 186 | 375.8 |
| 173.3 | 188 | 376.7 |
| 175.3 | 190 | 377.6 |
| 177.3 | 192 | 378.5 |
| 179.3 | 194 | 379.3 |
| 181.3 | 196 | 380.2 |
| 183.3 | 198 | 381.0 |
| 185.3 | 200 | 381.9 |
| 190.3 | 205 | 384.0 |
| 195.3 | 210 | 386.0 |
| 200.3 | 215 | 388.0 |
| 205.3 | 220 | 389.9 |
| 210.3 | 225 | 391.9 |
| 215.3 | 230 | 393.8 |
| 220.3 | 235 | 395.6 |
| 225.3 | 240 | 397.4 |
| 230.3 | 245 | 399.3 |
| 235.3 | 250 | 401.1 |
| 245.3 | 260 | 404.5 |
| 255.3 | 270 | 407.9 |
| 265.3 | 280 | 411.2 |
| 275.3 | 290 | 414.4 |
| 285.3 | 300 | 417.5 |

## Introduction

When selecting a butterfly valve for water applications you must first determine the requirements of the valve assembly. The first question to ask is, "Will the valve be used for "Isolation" or "Proportional Control" of the fluid?" and "Does the application require a 2-way or 3-way assembly?"

## 2-way and 3-way Isolation Valves

When selecting a valve for isolation purposes, it is seldom necessary to calculate flow requirements beyond the published Cvs (flow coefficients)* of the valve. These valves are typically line size and require the lowest pressure drop available in the full open position. It may be possible to supply a valve smaller than the actual line size and still obtain a low-pressure drop. However, the cost of reducing flanges will typically offset any savings incurred by reducing the valve size. The 2- and 3-way Flow Coefficient charts, below and on I-16, provide Cv values for Siemens butterfly valves.

## 2-way and 3-way Proportional Control Valves

Control Valves are the most important element of a fluid handling system and proper selection of these valves is crucial for efficient operation of the process. When sizing butterfly valves for control, it is imperative to have certain requirements of the system.

## You must have:

- Maximum flow requirement: This would be equivalent to the design flow and provided or converted to gallons per minute.
- Maximum pressure drop allowed: The Consulting Engineer usually provides this factor and are typically 3 to 5 psi max. However, the pressure drop should never exceed one half of the inlet pressure.
Without these two factors, selection of a control valve would be simply a guess.


## 2-way Flow Coefficients (Cvs)

| Size | Degrees Open |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ | $50^{\circ}$ | $60^{\circ}$ | $70^{\circ}$ | $80^{\circ}$ | $90^{\circ}$ |
| 2" | 0 | 1.3 | 5 | 14 | 26 | 40 | 52 | 59 | 60 |
| 2-1/2" | 0 | 1.4 | 6 | 21 | 44 | 74 | 107 | 138 | 151 |
| $3 "$ | 0.7 | 1.5 | 8 | 29 | 67 | 115 | 175 | 234 | 262 |
| 4" | 1.7 | 15 | 48 | 107 | 196 | 318 | 463 | 589 | 647 |
| $5 "$ | 3 | 32 | 99 | 206 | 362 | 579 | 832 | 1045 | 1141 |
| $6 "$ | 4 | 47 | 145 | 295 | 510 | 810 | 1160 | 1450 | 1580 |
| 8" | 6 | 84 | 239 | 450 | 751 | 1190 | 1754 | 2385 | 2892 |
| 10" | 9 | 133 | 360 | 652 | 1064 | 1683 | 2524 | 3596 | 4593 |
| 12" | 12 | 192 | 509 | 899 | 1449 | 2288 | 3470 | 5085 | 6682 |
| $14 "$ | 75 | 340 | 770 | 1400 | 2200 | 3400 | 5600 | 7900 | 10000 |
| $16 "$ | 100 | 440 | 1000 | 1800 | 2800 | 4500 | 7400 | 10800 | 13000 |
| 18" | 130 | 570 | 1300 | 2300 | 3600 | 5800 | 9600 | 15000 | 18000 |
| 20" | 150 | 710 | 1600 | 2900 | 4600 | 7200 | 12000 | 18400 | 22000 |

Table Note

- Flow Coefficients $(\mathrm{Cv})=$ The amount of water in gallons per minute, at $60^{\circ} \mathrm{F}$ that will pass through a given orifice with a one pound pressure drop.


## Butterfly Valves

## 3- way Flow Coefficients (Cvs)

| Size | Degrees Open |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Run | $0^{\circ}$ | $10^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ | $50^{\circ}$ | $60^{\circ}$ | $70^{\circ}$ | $80^{\circ}$ | $90^{\circ}$ |
| Branch | $90^{\circ}$ | $80^{\circ}$ | $70^{\circ}$ | $60^{\circ}$ | $50^{\circ}$ | $40^{\circ}$ | $30^{\circ}$ | $20^{\circ}$ | $10^{\circ}$ | $0^{\circ}$ |
| 2" | 54 | 53 | 49 | 43 | 38 | 40 | 44 | 52 | 57 | 58 |
| 2-1/2" | 114 | 108 | 93 | 74 | 52 | 64 | 78 | 102 | 126 | 135 |
| 3" | 188 | 178 | 148 | 114 | 55 | 95 | 120 | 165 | 210 | 229 |
| 4" | 385 | 374 | 348 | 313 | 150 | 295 | 345 | 419 | 482 | 511 |
| 5" | 642 | 627 | 600 | 563 | 270 | 549 | 630 | 740 | 829 | 870 |
| $6 "$ | 935 | 909 | 867 | 809 | 483 | 780 | 895 | 1051 | 1180 | 1242 |
| 8" | 1688 | 1573 | 1424 | 1271 | 796 | 1175 | 1367 | 1661 | 1994 | 2254 |
| 10" | 2667 | 2430 | 2132 | 1856 | 1142 | 1685 | 1971 | 2439 | 3046 | 3570 |
| 12" | 3938 | 3531 | 3019 | 2579 | 1629 | 2312 | 2715 | 3401 | 4368 | 5240 |
| 14" | 5109 | 4825 | 4416 | 3719 | 2433 | 3514 | 3992 | 5259 | 6342 | 7173 |
| $16 "$ | 6735 | 6462 | 5832 | 4904 | 3213 | 4498 | 5265 | 6943 | 8567 | 9410 |
| 18" | 9060 | 8724 | 7650 | 6372 | 4433 | 5778 | 6815 | 9056 | 11695 | 12785 |
| 20" | 11229 | 10799 | 9545 | 7901 | 5619 | 7339 | 8449 | 11309 | 14423 | 15770 |

## Table Notes

- Three-way valve assemblies Cvs are corrected from published two-way Cvs to account for line losses generated by the tee, and are calculated values only. The pipe friction losses are a function of fluid velocity through the pipe and the three-way Cvs listed are apparent for full flow through the pipe. Operation at less than full capacity (lower velocity) will increase the actual Cvs


## Sizing Example

With this information and assuming the media is water or a similar media (glycol/water mix), a control valve can be properly sized for the application by following these steps:

1. Calculate the required Cv : Using the following formula and the information required above, you could calculate the flow coefficient ( Cv ) of the control valve.


Whereas: GPM = The maximum flow requirement $\mathrm{P}=$ The max. pressure drop ( 5 psi )

## Example

The line size is 6 " and the required flow is 600 GPM with a maximum pressure drop of 5 psi . The square root of 5 is equal to 2.236. When divided into 600, the required Cv for this application is: 268.336 .
2. Select your valve size: Using the Flow Coefficients (Cvs), select the appropriate valve size. If your required Cv is in between valve sizes, choose the larger size valve. When selecting a 3-way assembly, the Cv of the run should be selected.

## Example

The line size is 6 " and the calculated required Cv is 268.336. The valve selected is a 4 " with a rated Cv of 647.

Butterfly valves are high capacity valves and require very little pressure drop to control flow, which allows for reduction from the line size when sizing valves. This pipe reduction affects the flow characteristics and will reduce the effective Cv of the valve. This phenomenon is known as the piping geometry factor $(\mathrm{Fp})$, which brings us to the final step in valves sizing.
3. Piping Geometry Factor: Reducing pipe sizes for installation of a smaller than pipe size valves will reduce the effective Cv of the valve. The greater the pipe reduction, the greater loss of Cv. Using the Adjusted Cvs for Piping Geometry Factors chart, verify that the corrected Cv, for the valve size selected, meets or exceeds the required Cv calculated in step 2.
Note: 3-way Cvs have already been adjusted.

## Adjusted Cvs for Piping Geometry Factors

| Size | Pipe Size |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2-1/2" | 3" | 4" | 5" | 6" | 8" | 10" | 12" | 14" | 16" | 18" | 20" | 22" | 24" |
| 2" | 47 | 38 |  |  |  |  |  |  |  |  |  |  |  |  |
| 2-1/2" |  | 125 | 79 |  |  |  |  |  |  |  |  |  |  |  |
| 3" |  |  | 189 | 149 |  |  |  |  |  |  |  |  |  |  |
| 4" |  |  |  | 505 | 408 |  |  |  |  |  |  |  |  |  |
| 5" |  |  |  |  | 947 | 685 |  |  |  |  |  |  |  |  |
| $6 "$ |  |  |  |  |  | 1138 | 916 |  |  |  |  |  |  |  |
| 8" |  |  |  |  |  |  | 2256 | 1822 |  |  |  |  |  |  |
| 10" |  |  |  |  |  |  |  | 3812 | 3123 |  |  |  |  |  |
| 12" |  |  |  |  |  |  |  |  | 5747 | 4811 |  |  |  |  |
| 14" |  |  |  |  |  |  |  |  |  | 8900 | 7600 |  |  |  |
| 16" |  |  |  |  |  |  |  |  |  |  | 11830 | 10140 |  |  |
| 18" |  |  |  |  |  |  |  |  |  |  |  | 16560 | 14580 |  |
| 20" |  |  |  |  |  |  |  |  |  |  |  |  | 20460 | 18260 |

6-inch 3-way Assembly at Constant Valve Differential Pressure
(corrected for tee loss)


## SIEMENS

## Terminology

Absolute Pressure - Absolute pressure is referenced to a theoretical perfect vacuum. At standard atmospheric pressure, absolute pressure may be calculated by adding 14.7 psi to the observed gauge pressure.

Ambient Temperature Rating - Ambient temperature refers to the temperature of the air surrounding the device.
Angled Body - A two way valve body that has connection points at right angles to each other.

Butterfly Valve - A valve utilizing a disk rotating on a shaft to provide control and close off. Alternately, a check valve utilizing two semi-circular hinged plates to permit flow in one direction only.

Booster Pump - A pump used in secondary loops of hydronic systems to provide additional flow for that section of the system.

Cavitation - The forming and imploding of cavities in a liquid due to rapid pressure changes, producing shock waves and cyclic stresses that can lead to undesirable noise and/or surface fatigue damage.

Close-off Rating - The maximum differential pressure, inlet to outlet, that a valve will close off against while fluid is flowing to a given leakage rate (tightness) criteria. In a stroke valve, the primary determinants are the force available from the actuator, the diameter of the plug, and the valve design. In a rotary valve, such as a ball valve, the primary determinant is typically the seal design as the torque of the actuator has little effect.

Close-off Rating of Three Way Valves - The maximum pressure difference between either of the two inlet ports and the outlet port for mixing valves, or the pressure difference between the inlet port and either of the two outlet ports for diverting valves.

Contoured Plug - In a globe valve, a contoured plug uses its peripheral shape to affect a desired flow characteristic. This is typically linear, equal percentage, or a modification of these. These are differentiated from V-plugs, basket plugs, cage plugs, and the like by the fact that the media flows around the plug and not through it.
Controlled Medium - The controlled medium is the material that is being conveyed and controlled though the device. In typical HVAC systems this includes air, water, and/or steam. It may also include fuel oil, natural gas, refrigerants, etc.
Critical Pressure Drop - The maximum pressure drop across a valve at which gasses and vapors will follow standard flow calculations. Pressure drops greater than this produced what is known as "choked flow" and sizing criteria will no longer accurately predict the volumetric flow.

Design Conditions - The assumed environmental variables that define the performance limits required of a HVAC system. This may include maximum and minimum outside air temperatures, expected solar and other thermal loads, occupancy levels, etc.
Direction of Flow - The flow of a controlled fluid through the valve is usually represented by an arrow on the valve body. If the flow of the fluid goes against the indicated direction, the disk can slam into the seat as it approaches the closed position. The result is excessive wear, hammering, and oscillations. Additionally the actuator must work harder to reopen the closed valve since it must overcome the pressure exerted by the fluid on top of the disc, rather than have the fluid assist in opening the valve by exerting pressure under the disc.
Diverting Valve - A three way valve that has one inlet and two outlets. Water entering the inlet port is diverted to either of the two outlet ports in any proportion desired by moving the valve stem. These valves are not commonly use in modern control loops.

End Fitting - The part of the valve body that connects to the piping. Union, screwed, flared, sweat and flanged are typical examples of end fittings.
Equalinear Flow - Valve Cv vs travel position is approximately mid-way between that of linear and equal percentage.
Equal Percentage Flow Characteristic - An equal percentage flow characteristic is one in which a flow rate change is proportional to the flow rate just prior to the change in valve position. Equal increments of valve travel result in equal percentage changes to the existing flow rate. Flow capacity increases exponentially with valve stem travel.

Flanged End Connections - A valve that connects to a pipe by bolting a flange on the valve to a flange on the pipe. Flanged connections are often used on larger valves, typically over 2 ".

Flashing - In the context of control valves, flashing is related to cavitation, but the mechanics are slightly different. Flashing occurs when a liquid's environment causes a rapid phase change from liquid to gaseous phases. With flashing, the volume of vapor is much greater than the volume of liquid, and rapidly accelerates the remaining liquid droplets, which forcefully impact the mechanical components of the valve and pipes, causing damage. This situation can be calculated by knowing the pressures and temperatures involved, as well as the vapor pressure of the liquid at those temperatures. Cavitation often occurs in environments that have not yet reached the point of flashing, due to fluid flow dynamics and velocities.

## Terminology

Flow Characteristic - The relation between volumetric flow and valve position.

Flow Coefficient - The flow coefficient is the constant that relates volumetric flow, differential pressure, and specific gravity of a fluid through a metering device. Cv is the flow coefficient in imperial units. For liquids through a standard orifice it is calculated to be equal to the volumetric flow in gallons per minute times the square root of the specific gravity divided by the square root of the differential pressure in psi. For water systems the specific gravity can be assumed to be 1 , therefore it is often simplified to GPM divided by the square root of $\Delta P$. For HVAC applications, a control valve closely follows this orifice model.

Flow Rate - The volume of media conveyed per unit of time. Typical US units are gallons per minute (GPM) for water and pounds per hour (\#/hr) for steam.

FPM — Feet per minute.
Full Port — Maximum flow capacity possible for a particular ball valve orifice. In a ball valve, this typically refers to a valve with no flow characterizer or restrictor.

Gauge Pressure - Pounds per square inch (PSI) as read on a gauge face. This differs from Absolute Pressure in that it is relative to the current ambient pressure, not a fixed reference such as absolute vacuum. Gauge pressure, therefore, uses the local ambient pressure as its zero point (14.7 psia at sea level and standard conditions).

GPM — Gallons per minute.
Incompressible - Description of liquids, because their change in volume due to pressure is negligible.
Laminar Flow - Also known as viscous or streamlined flow. A non-turbulent flow regime in which the stream filaments glide along the pipe axially with essentially no transverse mixing. This is usually associated with viscous liquids. The area inside a valve is typically turbulent - the opposite of laminar.

Load - A demand on the mechanical equipment in an HVAC system.
Load Change - A change in the building cooling or heating requirements as a result of air temperature variations, caused by wind, occupants, lights, machinery, solar effect, etc.

Mixing Valve - A three way valve having two inlets and one outlet. The proportion of fluid entering each of the two inlets can be varied by moving the valve stem. These valves are typically not suitable for diverting applications.

Normally Closed (N.C.) - Condition of the valve upon loss of power or control signal to the actuator. Also as relates to a stroke valve body that has been manufactured as a N.C. valve body. In stroke valves, this is typically the valve's state when the stem is in the "up" position.

Normally Open (N.O.) - Condition of the valve upon loss of power or control signal to the actuator. Also as relates to a stroke valve body that has been manufactured as a N.O. valve body. In stroke valves, this is typically the valve's state when the stem is in the "up" position.
NPT - A pipe thread standard describing tapered pipe threads, common in North America (National Pipe thread Tapered).

Packing - Seals used around the valve stem so that the controlled medium will not leak outside the valve.

Port - Opening (inlet or outlet) that allows flow through a valve body.

Positive Positioner - A device that eliminates the actuator shaft positioning error due to load on the valve body. This device is closed loop, and applies the necessary force required to positively position the valve stem to a referenced (commanded) position.
Pressure Drop - The difference in pressure between the inlet and outlet ports of the control valve, commonly refered to as $\Delta P$ (delta $P$ ).

PSI - Pounds per square inch.
PSIA - Pounds per square inch absolute.
(Also see Absolute Pressure.)
PSIG - Pounds per square inch gauge.
(Also see Gauge Pressure.)
Rangeability - The ratio of the maximum controllable flow to the minimum controllable flow. As an example, a valve with a rangeability of 50 to 1 having a total flow capacity of 100 GPM, fully open, will be able to control flow accurately down to 2 GPM.

Reduced port - A smaller flow capacity that is possible for the particular end fitting.

Reducer - A pipe fitting that is used to couple a pipe of one size to a pipe of a different size. An increaser may be used when the pipe sizes are reversed.

Saturated Steam - Steam which is at its lowest possible temperature at a given pressure without a phase change to liquid.

Screwed- end connection - A valve body with a threaded pipe connection, usually female NPT threads, in valve bodies through 2 ".

## Terminology

Seat - The stationary portion of the valve which seals the valve, thus prevents flow, when in full contact with the movable ball, plug or disc.

Static Pressure rating - The maximum pressure that the valve body will tolerate per a defined standard. The standards may define the pressure at temperatures other than that observed, so one must understand the standard to understand the actual pressure rating for the given application. Common pressure standards for HVAC valves in North America include ANSI $(125,250)$ and WOG $(300,600)$, but others such as CWP are sometimes used.

Stem - The cylindrical shaft of a control valve moved by an actuator, to which the throttling plug, ball or wafer disc is attached.

Stroke - The total distance that a linear valve stem travels or moves. It is also known as lift.

Superheated Steam - Steam at a temperature higher than saturation temperature at the given pressure.

System Pressure Drop - The sum of all pressure drops in a Hydronic system.

Three Way Valve - A valve body with one inlet and two outlets or two inlets and one outlet.

Tight Shut-off - A valve body with no flow or leakage in a closed position. This is relative to the defined tightness of the seal, usually defined by a measurement standard. The most common standard is ANSI/FCI $70-2$, which classifies "tightness" from Class I to Class VI. Class I is non-defined leakage, Class II through Class IV are descriptive based on leakage as a percent of total capacity, and Class V and Class VI are descriptive based on leakage as a finite rate per inch of orifice diameter. Since the criteria and testing method for Class II - IV are significantly different than Class V - VI, these groups cannot be directly compared.

Trim - All parts of the valve which are in contact with the flowing media, but are not part of the valve shell or casting. Ball, stem, disc, plug, and seat are all considered trim components.

Turndown - Ratio between the maximum usable flow and the minimum controllable flow. Turndown is usually less than Rangeability, and cannot be applied to a valve exclusive of the specific application it is placed in, It is a function of the valve, actuator, piping, coil, and all other system parameters that determine the maximum usable flow. Since the valve only has reasonable control over one part of the ratio, the minimum controllable flow, this is not a good criteria for evaluating valve quality.

Two-way Valve - A valve body with a single flow path one inlet and one outlet.

Valve - A control device which will vary the rate of flow of a medium such as water or steam.

Valve Actuator - A device that uses a source of power to position or operate a valve, sometimes also called a valve operator. The source of power may be anything, examples include manual (via a hand wheel), pneumatic, or electronic.

Valve Body - The portion of the valve casting through which a controlled medium flows.

Valve Disc - The movable part of a butterfly valve which makes contact with the seat when the valve is closed.

Valve Flow Characteristic - The relationship between the stem travel, expressed in percent of travel, and the flow of the fluid through the valve, expressed in percent of full flow or gallons per minute.

Valve Guide - The part of a globe valve throttling plug that keeps the disc aligned with the valve seat.

Velocity - The rate of movement for air or water, distance per unit time.

Viscous - Having a relatively high resistance to flow.
Volumetric Air Flow - Area x Velocity.
Wire Draw - The process where high velocity media erodes a path across the mechanical components of a valve. This typically occurs in a stroke valve when the valve is operated primarily with the plug very close to the seat, causing very high velocities of media across the plug and seat. The damage appears as if a wire has been drawn across the components. This differs from the other typical valve mechanical damage modes - cavitation and flashing - where the surface appears to have been pulled away as or struck by very small particles, respectively.

## Introduction

The size and quantity of actuators required depends on several damper torque factors:

- Type of damper seals (Standard, low or very low leakage)
- Quality of damper installation
- Number of damper sections
- Approach air velocity
- Static pressure

The following procedures can be used to determine the damper torque, actuator size and quantity of actuators required to operate a damper.

## Determing Damper Torque

1. From the damper manufacturer get the Damper Torque Rating (DTR) for the damper at the most severe operating conditions.
If the damper torque rating is not available,
Table 1 can be used for estimating purposes only on an interim basis. However, it is very important to get the damper torque rating from the manufacturer as soon as possible to assure accurate torque calculations.
2. Calculate the damper area (DA) in square feet from the damper dimensions.
3. Calculate the Total Damper Torque (TDT) in lb-in using the following formula:

## TDT = DTR X DA

4. If the damper torque rating is not available, use a torque wrench on the damper shaft while air is moving through the duct to measure the TDT.

## Actuator Size

1. From the actuator literature select the actuator type and size whose actuator torque rating (ATR) in lb-in is most appropriate for the application.
2. The ATR is normally based on $90^{\circ}$ rotation of the damper. For torque ratings of other than $90^{\circ} \mathrm{f}$ rotation, use the following formula:

$$
\begin{gathered}
\text { ATR @ X́rotation }= \\
\text { ATR @ } 90^{\circ} \text { rotation x }\left(\frac{\text { Crank Radius @ } \mathrm{X}^{\circ}}{\text { Crank Radius @ } 90^{\circ}}\right)
\end{gathered}
$$

3. If the actuator is rated in pounds of thrust, it can be converted to torque using the following formula:

Torque $=\left({ }^{*}\right.$ Crank arm length $\left.\times 0.707\right) \times$ Thrust
*The crank arm length is for $90^{\circ}$ shaft rotation at nominal actuator stroke.

## Quantity of Actuators

1. Calculate the number of actuators required using the following formula:
Number of actuators $=\frac{\text { Total Damper Torque }}{\text { SF }}$
SF = Safety Factor: When calculating the number of actuators required, a safety factor should be included for unaccountable variables such as slight misalignments, aging of the damper, etc. A suggested factor is 0.8 or $80 \%$ of the rated torque.
2. If the number of actuators calculated is too large to be practical, select a more powerful actuator or consider using a positioning relay if it is a pneumatic actuator.

Table 1

| Damper Type | Damper Leakage at 1" $\mathrm{H}_{2} \mathrm{O}$ Static Pressure Drop | Damper Torque for Approach Air Velocities of 1200 ft ./min. or less |
| :---: | :---: | :---: |
| Standard leakage | More than $10 \mathrm{CFM} / \mathrm{ft} .^{2}$ | $2.5 \mathrm{lb} .-\mathrm{in} . / \mathrm{ft} .^{2}$ |
| Low leakage | 5 to $10 \mathrm{CFM} / \mathrm{ft} .^{2}$ | $5.0 \mathrm{lb} .-\mathrm{in} . / \mathrm{ft} .^{2}$ |
| Very low leakage | Less than $5 \mathrm{CFM} / \mathrm{ft} .^{2}$ | $7.0 \mathrm{lb} .-\mathrm{in} . / \mathrm{ft} .^{2}$ |

Contact your local customer service representative for additional application assistance when specific damper factors are known.

| Type | Intended Use and Description | Requirements or Qualification Tests, Paragraph or Section Numbers |
| :---: | :---: | :---: |
| 1 | Indoor use primarily to provide a degree of protection against limited amounts of falling dirt | Corrosion Protection-5.3 or Rust ResistanceSection 38 |
| 2 | Indoor use primarily to provide a degree of protection against limited amounts of falling water and dirt. | Corrosion Protection-5.3 or Rust ResistanceSection 38, Drip-Section 31, Gaskets-Section 14 and Gasket Tests-Section 43 |
| 3 | Outdoor use primarily to provide a degree of protection against rain, sleet, wind blown dust and damage from external ice formation. <br> Sections 14, and Gasket Tests-Section 43 | Rain-Section 30, Outdoor Dust or HoseSection 32 or 35, Icing-Section 34, Protective Coating-Section 15, Gaskets- |
| 3R | Outdoor use primarily to provide a degree of protection against rain, sleet, and damage from external ice formation. | Rain-Section 30, Icing-Section 34, Protective Coating-Section 15, Gaskets-Section 14, and Gasket Tests-Section 43 |
| 3 S | Outdoor use primarily to provide a degree of protection against rain, sleet, windblown dust and to provide for operation of external mechanisms when ice laden. | Rain-Section 30, Outdoor Dust or HoseSection 32 or 35, Icing-Section 34, Protective Coating-Section 15, GasketsSections 14, and Gasket Tests-Section 43 |
| 4 | Indoor or outdoor use primarily to provide a degree of protection against windblown dust and rain, splashing water, hose-directed water and damage from external ice formation. | Hosedown-Section 35, Protective CoatingSection 15, Icing-Section 34, GasketsSection 34, and Gasket Tests-Section 43 |
| 4X | Indoor or outdoor use primarily to provide a degree of protection against corrosion, windblown dust and rain, splashing water, hose-directed water, and damage from | Hosedown-Section 35, Protective CoatingSection 15, Corrosion Resistance-Section 39, Icing-Section 34, Gaskets-Sections 14, and Gasket Tests-Section 43 |
| 5 | Indoor use primarily to provide a degree of protection against setting airborne dust, falling dirt, and dripping noncorrosive liquids. | Corrosion Protection-Section 5.3 or Rust Resistance-Section 38, Drip-Section 31, Indoor Setting Airborne Dust or Atomized Water Method B-Section 32 or 33, Gaskets-Sections 14, and Gasket Tests-Section 43 |
| 6 | Indoor or outdoor use primarily to provide a degree of protection against hose-directed water, and the entry of water during occasional temporary submersion at a limited depth Tests-Section 43 | Hosedown-Section 35, Icing-Section 34, Submersion-Section 36, Protective CoatingSection 15 Gaskets-Sections 14, and Gasket |
| 6P | Indoor or outdoor use primarily to provide a degree of protection against hose-directed water, the entry of water during prolonged submersion at a limited depth and damage from external ice formation. | Hosedown-Section 35, Icing-Section 34, Protective Coating-Section 15, Air PressureSection 40, Gaskets-Sections 14, and Gasket Tests-Section 43 |
| 12, 12K | Indoor use primarily to provide a degree of protection against circulating dust, falling dirt, and dripping noncorrosive liquids. Section 15 Drip-Section 31, Indoor Setting | Corrosion Protection-Section 5.3 or Rust Resistance-Section 38,Protective Coating- <br> Airborne Dust or Atomized Water Method BSection 32 or 33 , Gaskets-Sections 14, and Gasket Tests-Section 43 |
| 13 | Indoor use primarily to provide a degree of protection against dust, spraying of water, oil, and noncorrosive coolant. | Corrosion Protection-Section 5.3 or Rust Resistance-Section 38, Oil-Section 37, GasketsSections 14, and Gasket Tests-Section 43 |

## Table Notes

- Refer to specific sections in the UL Standard UL50 Enclosures for Electrical Equipment.
- NEMA Ratings can be applied by the manufacturer through a "self-certification" process or through an independent testing house, such as UL. The term, Type, indicates to an inspector that the certification was performed independently.

Multi-purpose, Balance-retard and Analog Relays

## Relay Piping

Application Index
In the list below locate the application and type of required to locate the appropriate connections diagram.

| Application | Type of Relay | Figure |
| :---: | :---: | :---: |
| Reverse Acting | Multi-purpose | 1 |
| Reverse Acting | Analog | 2 |
| Minimum Pressure | Multi-purpose | 3 |
| Minimum Pressure with Characterized Output | Multi-purpose | 4 |
| Minimum Pressure with Characterized Output | Analog | 5 |
| Characterized Minimum Pressure | Analog | 6 |
| Minimum Pressure with Hesitation | Balance-retard | 7 |
| Adjustable Minimum Pressure | Analog | 8 |
| Highest Pressure Signal Selector | Analog | 8 |
| Direct Acting | Multi-purpose | 9 |
| Direct Acting | Analog | 10 |
| Direct Acting with Positive Positioning Override | Analog | 11 |
| Signal Advancing | Multi-purpose | 12 |
| Adjustable Advancing | Analog | 13 |
| Summing | Analog | 13 |
| Signal Retard | Balance-retard | 14 |
| Signal Retard | Analog | 15 |
| Balancing | Balance-retard | 16 |
| Hesitation | Balance-retard | 17 |
| Averaging | Analog | 18 |
| Ratio 1 in = 2 out | Analog | 19 |
| Ratio 2 in = 1 out | Analog | 20 |
| Signal Inverting | Multi-purpose | 21 |
| Signal Inverting | Analog | 22 |
| Lowest Pressure Signal Selector | Multi-purpose | 23 |
| Lowest Pressure Signal Selector | Analog | 24 |
| Differential Pressure | Analog | 25 |
| Limit Control Direct Acting | Multi-purpose | 26 |
| Pressure Limiting in Dual Pressure Systems | Balance-retard | 27 |
| Limit Control Reverse Acting | Multi-purpose | 28 |



Figure 1.



Figure 3.


Figure 2.


Figure 4.

| Key |  |  |  |
| :--- | :--- | :--- | :--- |
| R | Output signal port | S | Air supply port |
| TD | Direct acting input signal port | SP | Setting of the adjustable screw |
| TR | Reverse acting input port | T | Direct acting input port |

(Continued—Refer to chart on I-23)




Figure 14.


Figure 15.


Figure 16.
(Continued—Refer to chart on I-23)



Figure 21.


Figure 22.


Figure 23.


Figure 25.



Figure 27.


Figure 28.

## SIEMENS

| Siemens | Honeywell | Johnson | Robertshaw | Barber-Colman | $\begin{aligned} & \text { Discontinued } \\ & \text { Siemens } \\ & \text { (Powers) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 243-0009 \\ & 243-0046 \end{aligned}$ <br> Reverse Acting | RP 972 A Reverse Acting | $C-208$ <br> Reverse Acting | R 516 <br> Reverse Acting | AK 50613 Reverse Acting | TYPE 783 Reverse Acting |
| $\begin{gathered} 243-0009 \\ 243-0046 \\ \text { Direct Acting } \end{gathered}$ | RP 970 A Direct Acting | C 5230 Direct Acting | R 532-L Direct Acting | AK-50603 Direct Acting |  <br> Type 782 Direct Acting |
| $\begin{aligned} & 243-0009 \\ & 243-0046 \end{aligned}$ <br> Minimum Pressure | SP 970 A Minimum Pressure | C 5230 Minimum Pressure | S511-5 Minimum Pressure | AK-50605 <br> Minimum Pressure | Type 782 Minimum Pressure |
| $\begin{gathered} 243-0010 \\ 243-0047 \\ \text { Balancing Relay } \end{gathered}$ | NONE | C 130-1 Balancing Relay | NONE | NONE |  |
|  | RP 971 A 1007 Sequencing Relay (Setpoint + 3 psig) | $\begin{gathered} \text { C 202-1 } \\ 1 \text { In }=2 \text { Out } \end{gathered}$ | R 539 $1 \text { in }=2 \text { Out }$ | $\begin{aligned} & A K-50703 \\ & 1 \mathrm{In}=2 O \mathrm{O} \end{aligned}$ | Type 782-0070 1 in = 2 Out |


| To Convert From | Into | Multiply By |
| :---: | :---: | :---: |
| atmospheres | feet of water (at $4^{\circ} \mathrm{C}$ ) | 33.90 |
| atmospheres | inch of mercury (at $0^{\circ} \mathrm{C}$ ) | 29.92 |
| atmospheres | pounds/square inch | 14.70 |
| Btu | foot-pounds | 778.3 |
| Btu | horsepower-hours | $3.931 \times 10^{-4}$ |
| Btu | kilowatt-hours | $2.928 \times 10^{-4}$ |
| Btu/hour | foot-pounds/second | 0.2162 |
| Btu/hour | horsepower-hours | $3.929 \times 10^{-4}$ |
| Btu/hour | watts | 0.2929 |
| Btu/minute | foot-pounds/second | 12.96 |
| Btu/minute | horsepower | 0.02356 |
| Btu/minute | kilowatts | 0.01757 |
| Btu/minute | watts | 17.57 |
| Btu/minute | tons of refrigeration | 1/200 |
| Btu/hour | tons of refrigeration | 1/12,000 |
| Btu/ft. ${ }^{2}$ /minute | Watts/square inch | 0.1221 |
| Btu/pound air | Kilojoules/kilogram | 2.33 |
| Candle/in. ${ }^{2}$ | Laberts | 0.4870 |
| Candle/ft. ${ }^{2}$ | Candle meters | 0.0929 |
| cubic feet | cubic inches | 1,728.0 |
| cubic feet | cubic yards | 0.03704 |
| cubic feet | gallons (U.S. liquid) | 7.48052 |
| cubic feet | pints (U.S. liquid) | 59.84 |
| cubic feet | quarts (U.S. liquid) | 29.92 |
| cubic feet/min. | gallons/second | 0.1247 |
| cubic feet/min. | pounds of water/minute | 62.43 |
| cubic feet/min. | liters per second | 0.4719 |
| cubic feet/sec. | millions gallons/day | 0.646317 |
| cubic feet/sec. | gallons/minute | 448.831 |
| cubic inches | cubic feet | $5.787 \times 10^{-4}$ |
| cubic inches | cubic yards | $2.143 \times 10^{-5}$ |
| cubic inches | gallons | $4.329 \times 10^{-3}$ |
| cubic yards | cubic feet | 27.0 |
| cubic yards | cubic inches | 46,656.0 |
| cubic yards | gallons (U.S. liquid) | 202.0 |
| cubic yards | pints (U.S. liquid) | 1,615.9 |
| cubic yards | quarts (U.S. liquid) | 807.9 |
| cubic yards/min. | cubic feet/second | 0.45 |
| cubic yards/min. | gallons/second | 3.367 |
| degrees (angle) | seconds | 3,600.0 |
| degrees/second | revolutions/minute | 0.1667 |


| To Convert From | Into | Multiply By |
| :---: | :---: | :---: |
| feet of water | atmospheres | 0.02950 |
| feet of water | inch of mercury | 0.8826 |
| feet of water | pounds/square foot | 62.43 |
| feet of water | pounds/square inch | 0.4335 |
| feet/min. | feet/second | 0.01667 |
| feet/min. | miles/hour | 0.01136 |
| feet/sec. | miles/hour | 0.6818 |
| feet/sec. | miles/min. | 0.01136 |
| Foot-candle | Lumen/square meter | 10.764 |
| foot-pounds | Btu | $1.286 \times 10^{-3}$ |
| foot-pounds | horsepower-hour | $5.050 \times 10^{-7}$ |
| foot-pounds | kilowatt-hour | $3.766 \times 10^{-7}$ |
| foot-pounds/min. | Btu/min. | $1.286 \times 10^{-3}$ |
| foot-pounds/min. | foot-pounds/second | 0.01667 |
| foot-pounds/min. | horsepower | $3.030 \times 10^{-5}$ |
| foot-pounds/min. | kilowatts | $2.260 \times 10^{-5}$ |
| foot-pounds/sec. | Btu/hour | 4.6263 |
| foot-pounds/sec. | Btu/min. | 0.07717 |
| foot-pounds/sec. | horsepower | $1.818 \times 10^{-3}$ |
| foot-pounds/sec. | kilowatts | $1.356 \times 10^{-3}$ |
| gallons | cubic feet | 0.1337 |
| gallons | cubic inches | 231.0 |
| gallons | cubic yards | $4.951 \times 10$ |
| gallons | liters | 3.785 |
| gallons (liq. Br. Imp.) | gallons (U.S. liquid) | 1.20095 |
| gallons (U.S.) | gallons | 0.83267 |
| gallons of water | pounds of water | 8.3453 |
| gallons/min. | cubic feet/sec. | $2.228 \times 10^{-3}$ |
| gallons/min. | cubic feet/hour | 8.0208 |
| US gallons/min. | liters per second | 0.06309 |
| US gallons/min. | liters per second | 3.7854 |
| gallons/hour | cubic meters/hour | $1.434 \times 10^{-3}$ |
| horsepower | Btu/minute | 42.44 |
| horsepower | foot-pounds/min. | 33,000.0 |
| horsepower | foot-pounds/sec. | 550.0 |
| horsepower | kilowatts | 0.7457 |
| horsepower | Watts | 745.7 |
| horsepower (boiler) | Btu/hour | 33.479 |
| horsepower (boiler) | kilowatts | 9.803 |
| horsepower-hours | Btu | 2,547.0 |
| horsepower-hours | foot-pounds | $1.98 \times 10^{6}$ |
| horsepower-hours | kilowatt-hours | 0.7457 |


| To Convert | Into | Multiply By |
| :---: | :---: | :---: |
| inch | Pa | 248.84 |
| inches | yards | $2.778 \times 10^{-2}$ |
| inches of mercury | atmospheres | 0.03342 |
| inches of mercury | feet of water | 1.133 |
| inches of mercury | pounds/square feet | 70.73 |
| inches of mercury | pounds/square feet | 0.4912 |
| inches of water | atmospheres | $2.458 \times 10^{-3}$ |
| inches of water | inches of mercury | 0.07355 |
| in. of water (at $4^{\circ} \mathrm{C}$ ) | ounces/square inches | 0.5781 |
| inches of water | pounds/square feet | 5.204 |
| inches of water | pounds/square inches | 0.03613 |
| kilometers | miles | 0.6214 |
| kilometers | yards | 1,094.0 |
| kilowatts | Btu/minutes | 56.92 |
| kilowatts | foot-pounds/minutes | $4.426 \times 10^{4}$ |
| kilowatts | foot-pounds/second | 737.6 |
| kilowatts | horsepower | 1.341 |
| kilowatts | Watt | 1,000.0 |
| kilowatts | Btu | 3,413.0 |
| kilowatts-hour | foot-pounds | $2.655 \times 10^{6}$ |
| kilowatts-hour | horsepower-hour | 1.341 |
| kilowatts-hour | pounds of water evaporated from and at $212^{\circ} \mathrm{F}$ | 3.53 |
| liters per sec. | US gal/min. | 15.85 |
| lumens/square feet | foot-candles | 1.0 |
| Lumen | Spherical candle power | 0.07958 |
| Lumen | Watt | 0.001496 |
| Lumen/square feet | Lumen/square meters | 10.76 |
| lux | foot-candles | 0.0929 |
| lux | btu/hr. | 1000 |
| meter | inches | 39.372 |
| meters | feet | 3.281 |
| meters | yards | 1.094 |
| miles/hour | feet/minute | 88.0 |
| miles/hour | feet/second | 1.467 |
| miles/hour | miles/minute | 0.1667 |
| miles/minute | feet/second | 88.0 |
| miles/minute | miles/hour | 60.0 |


| To Convert | Into | Multiply By |
| :---: | :---: | :---: |
| OHM (international) | OHM (absolute) | 1.0005 |
| ounces | pounds | 0.0625 |
| pounds | ounces | 16.0 |
| pounds of water | cubic feet/second | 0.01602 |
| pounds of water | cubic inches | 27.68 |
| pounds of water | gallons | 0.1198 |
| pounds of water/min. | cubic feet/second | $2.670 \times 10^{-4}$ |
| pounds/cubic feet | pounds/cubic inches | $5.787 \times 10^{-4}$ |
| pounds/cubic inches | pounds/cubic feet | 1,728.0 |
| pounds/square feet | atmospheres | $4.725 \times 10^{-4}$ |
| pounds/square feet | feet of water | 0.01602 |
| pounds/square feet | inches of mercury | 0.01414 |
| pounds/square feet | pounds/square inches | $6.944 \times 10^{-3}$ |
| pounds/square inch | atmospheres | 0.06804 |
| pounds/square inch | feet of water | 2.307 |
| pounds/square inch | inches of mercury | 2.036 |
| pounds/square inch | pounds/square feet | 144.0 |
| revolutions | degrees | 360.0 |
| square feet | square inches | 144.0 |
| Watts | Btu/hour | 3.4129 |
| Watts | Btu/minute | 0.05688 |
| Watts | foot-pounds/minute | 44.27 |
| Watts | foot-pounds/second | 0.7378 |
| Watts | horsepower | $1.341 \times 10^{-3}$ |
| Watts | kilowatts | 0.001 |
| Watt-hours | Btu | 3,413.0 |
| Watt-hours | foot-pounds | 2,656.0 |
| Watt-hours | horsepower-hour | $1.341 \times 10^{-3}$ |
| Watt-hours | kilowatt-hour | 0.001 |


| Quantity | To Convert From | Into | Multiply By |
| :---: | :---: | :---: | :---: |
| Area | Square Inches (in. ${ }^{2}$ ) | Square Centimeters ( $\mathrm{cm}^{2}$ ) | 6.4516 |
|  | Square Feet ( $\mathrm{ft} .^{2}$ ) | Square Meters ( $\mathrm{m}^{2}$ ) | $9.2903 \times 10^{-2}$ |
| Enthalpy/Heat | BTU Per Pound-Mass- ${ }^{\circ} \mathrm{F}$ (BTU/lb. $\mathrm{x}^{\circ} \mathrm{F}$ ) | Kilojoule Per Kilogram—Kelvin (kJ/kg.K) | 4.1840 |
| Flow ${ }^{1}$ | Cubic Inches Per Minute (in. ${ }^{3} / \mathrm{min}$.) | Cubic Centimeters Per Second ( $\mathrm{cm}^{3} / \mathrm{s}$ ) | 0.2731 |
|  | Cubic Feet Per Minute (ft. ${ }^{3} / \mathrm{min}$.) | Cubic Centimeters Per Second ( $\mathrm{cm}^{3} / \mathrm{s}$ ) | 471.9474 |
|  | Cubic Feet Per Minute ( $\mathrm{ft} .^{3} / \mathrm{min}$.) | Cubic Decimeters Per Second ( $\mathrm{dm}^{3} / \mathrm{s}$ ) $\left.=1 \mathrm{~s}\right)^{3}$ | 0.4719 |
|  | Cubic Feet Per Minute ( $\mathrm{ft} .^{3} / \mathrm{min}$.) | Cubic Meters Per Second ( $\mathrm{m}^{3} / \mathrm{s}$ ) | $0.4719 \times 10^{-3}$ |
|  | Cubic Feet Per Minute (ft. ${ }^{3} / \mathrm{min}$.) | Cubic Meters Per Hour ( $\mathrm{m}^{3} / \mathrm{h}$ ) | 1.6990 |
|  | Standard Cubic Feet Per Minute SCFM 60º, 14.7 psia | Cubic Meters Per Hour ( $\mathrm{m}^{3} / \mathrm{h} 0^{\circ} \mathrm{C}, 1.01325 \mathrm{bar}$ ) | $\begin{aligned} & 1.695 \\ & 1.607 \end{aligned}$ |
|  | Standard Cubic Feet Per Minute SCFM 60F, 14.7 psia | Cubic Meters Per Hour ( $\mathrm{m}^{3} / \mathrm{h} 15^{\circ} \mathrm{C}, 1.01325 \mathrm{bar}$ ) | 1.695 |
|  | Gallons Per Minute (U.S. liquid) (GPM) | Cubic Decimeters Per Seconds ( $\mathrm{dm}^{3} / \mathrm{s}$ ) $=1 / \mathrm{s}$ ) | 0.0631 |
| Force | Pound (Force) (lb.) | Newtons (N) | 4.4482 |
| Length | Inches (in.) | Millimeters (mm) | 25.4000 |
|  | Inches (in.) | Centimeters (cm) | 2.5400 |
|  | Feet (ft.) | Centimeters (cm) | 30.4800 |
|  | Feet (ft.) | Meters (m) | 0.3048 |
| Mass (Weight) ${ }^{2}$ | Pound (lb.) | Kilogram (kg) | 0.4536 |
| Power | BTU Per Hour (BTU/hr.) | Watts (W) | 0.2929 |
|  | Horsepower (hp) | Watts (W) | 746.0000 |
| Pressure (Stress) | Pounds Per Square Inch (psi) | Kilopascals (kPa) | 6.8947 |
|  | Kilograms Per Square Centimeters ( $\mathrm{Kg} / \mathrm{cm}^{2}$ ) | Kilopascals (kPa) | 98.0665 |
|  | Inches of Water (" W.G.) @ 60% | Pascals (Pa) | 248.84 |
|  | Inches of Mercury (" H.G.) @ 60F | Pascals (Pa) | 3376.85 |
| Toruqe (Bending) | Degrees Fahrenheit ( ${ }^{\circ} \mathrm{F}$ ) | Degrees Celcius ( $\mathrm{t}^{\circ} \mathrm{C}$ ) | $\mathrm{t}^{\circ} \mathrm{C}=\frac{\left(\mathrm{t}^{\circ} \mathrm{F}-32\right)}{1.8}$ |
|  | Degrees Fahrenheit ( ${ }^{\circ} \mathrm{F}$ ) | Kelvin (tK) | $\mathrm{tK}=\frac{\left(\mathrm{t}^{\circ} \mathrm{F}+459.67\right)}{1.8}$ |
| Torque | Pound Force-Inch (lb.-in.) | Newton-Meter (Nm) | 0.1129 |
|  | Pound Force-Foot (lb.-ft.) | Newton-Meter (Nm) | 1.3558 |
| Velocity | Feet Per Second (ft./sec.) | Meters Per Second (m/s) | 0.3048 |
|  | Feet Per Minute (ft./min.) | Meters Per Second ( $\mathrm{m} / \mathrm{s}$ ) | $5.0800 \times 10^{-3}$ |
|  | Miles Per Hour (MPH) | Meters Per Seond (m/s) | 0.4470 |
| Volume | Cubic Inches (in. ${ }^{3}$ ) | Cubic Centimeters ( $\mathrm{cm}^{3}$ ) | 16.3871 |
|  | Cubic Feet ( $\mathrm{ft} .^{3}$ ) | Cubic Meters $\left(\mathrm{m}^{3}\right)=$ Stere | 2,8317 $\times 10^{-2}$ |
|  | Gallons U.S. (gal.) | Cubic Meters $\left(\mathrm{m}^{3}\right)=$ Stere | $3.7854 \times 10^{-3}$ |
|  | Ounce (oz.) | Cubic Meters $\left(\mathrm{m}^{3}\right)=$ Stere | $2.9573 \times 10^{-5}$ |
| Work (Energy) | BTU (BTU) | Kilojoule (kJ) | 1.0551 |
|  | Foot Pound (ft.-lb.) | Joule (J) | 1.3558 |
|  | Watthour (W-hr.) | Kilojoule (kJ) | 3.6000 |

Chart Notes

1. Since standard and normal cubic meters (STD $\mathrm{m}^{3}$ and $\mathrm{Nm}^{3}$ ) do not have a universally accepted definition, their reference pressure and temperature should always be spelled out.
2. In commercial and everyday use, the term weight almost always means mass.
3. Air consumption for pneumatic control devices should be expressed in milliliters per second ( $\mathrm{ml} / \mathrm{s}$ ).

Allowable leakage rates for pneumatic control devices should be expressed in milliliter per second ( $\mathrm{ml} / \mathrm{s}$ ) or microliters per second (ul/s).

## SIEMENS

## Instructions

The index numbers in bold face refer to the pressure either in psi or kilopascals ( kPa ) which it is desired to convert into the other scale. If converting from psi to kPa the equivalent pressure will be found in the left column, while if converting from kPa to psi , the equivalent pressure will be found in the column on the right.
Example: Index $1515 \mathrm{psi}=103.421 \mathrm{kPa} .15 \mathrm{kPa}=2.176 \mathrm{psi}$
By manipulation of the decimal point, this table may be extended to values below or above 100 .

| kPa | Index |  |
| :---: | :---: | :---: |
| 0.000 | 0 | 0.000 |
| 6.895 | 1 | 0.145 |
| 16.789 | 2 | 0.290 |
| 20.684 | 3 | 0.435 |
| 27.579 | 4 | 0.580 |
| 34.474 | 5 | 0.725 |
| 41.368 | 6 | 0.870 |
| 48.263 | 7 | 1.015 |
| 55.158 | 8 | 1.160 |
| 62.053 | 9 | 1.305 |
| 68.948 | 10 | 1.450 |
| 75.842 | 11 | 1.595 |
| 82.737 | 12 | 1.740 |
| 89.632 | 13 | 1.885 |
| 96.527 | 14 | 2.030 |
| 103.421 | 15 | 2.176 |
| 110.316 | 16 | 2.321 |
| 177.211 | 17 | 2.466 |
| 124.106 | 18 | 2.611 |
| 131.000 | 19 | 2.756 |
| 137.895 | 20 | 2.901 |
| 144.790 | 21 | 3.046 |
| 151.685 | 22 | 3.191 |
| 158.579 | 23 | 3.336 |
| 165.474 | 24 | 3.481 |
| 172.369 | 25 | 3.626 |


| $\mathrm{psi}^{\mathrm{kPa}}$ | Index |  |
| :---: | :---: | :---: |
| 179.264 | 26 | 3.771 |
| 186.058 | 27 | 3.916 |
| 193.053 | 28 | 4.061 |
| 199.948 | 29 | 4.206 |
| 206.843 | 30 | 4.351 |
| 213.737 | 31 | 4.496 |
| 220.632 | 32 | 4.641 |
| 227.527 | 33 | 4.786 |
| 234.422 | 34 | 4.931 |
| 241.316 | 35 | 5.076 |
| 248.211 | 36 | 5.221 |
| 255.106 | 37 | 5.366 |
| 262.001 | 38 | 5.511 |
| 268.895 | 39 | 5.656 |
| 275.790 | 40 | 5.801 |
| 282.685 | 41 | 5.946 |
| 289.580 | 42 | 6.092 |
| 296.475 | 43 | 6.237 |
| 303.369 | 44 | 6.382 |
| 310.264 | 45 | 6.527 |
| 317.459 | 46 | 6.672 |
| 324.054 | 47 | 5.617 |
| 330.948 | 48 | 6.962 |
| 337.843 | 49 | 7.107 |
| 344.729 | 50 | 7.252 |


| kPa | Index | psi |
| :---: | :---: | :---: |
| 531.633 | 51 | 7.397 |
| 358.527 | 52 | 7.542 |
| 365.422 | 53 | 7.687 |
| 372.317 | 54 | 7.832 |
| 379.212 | 55 | 7.977 |
| 386.106 | 56 | 8.122 |
| 393.001 | 57 | 8.267 |
| 399.896 | 58 | 8.412 |
| 406.791 | 59 | 8.557 |
| 413.685 | 60 | 8.702 |
| 420.580 | 61 | 8.847 |
| 427.475 | 62 | 8.992 |
| 434.370 | 63 | 9.137 |
| 441.264 | 64 | 9.282 |
| 448.159 | 65 | 9.427 |
| 455.054 | 66 | 9.572 |
| 431.949 | 67 | 9.717 |
| 468.843 | 68 | 9.862 |
| 475.738 | 69 | 10.008 |
| 482.633 | 70 | 10.153 |
| 489.528 | 71 | 10.298 |
| 496.422 | 42 | 10.443 |
| 503.317 | 73 | 10.588 |
| 510.212 | 74 | 10.733 |
| 517.107 | 75 | 10.878 |


| kPa | Index | psi |
| :---: | :---: | :---: |
| 524.001 | 76 | 11.023 |
| 530.896 | 77 | 11.168 |
| 537.791 | 78 | 11.313 |
| 544.686 | 79 | 11.458 |
| 551.581 | 80 | 11.603 |
| 558.475 | 81 | 11.748 |
| 565.370 | 82 | 11.893 |
| 572.265 | 83 | 12.038 |
| 579.160 | 84 | 12.183 |
| 586.054 | 85 | 12.328 |
| 592.949 | 86 | 12.473 |
| 599.844 | 87 | 12.618 |
| 606.739 | 88 | 12.763 |
| 613.633 | 89 | 12.908 |
| 621.528 | 90 | 13.053 |
| 627.423 | 91 | 13.198 |
| 634.318 | 92 | 13.343 |
| 641.212 | 93 | 13.488 |
| 648.107 | 94 | 13.633 |
| 655.002 | 95 | 13.778 |
| 661.897 | 96 | 13.924 |
| 668.791 | 97 | 14.069 |
| 675.686 | 98 | 14.214 |
| 682.581 | 99 | 14.359 |
| 689.476 | 100 | 14.504 |

All values rounded to 0.001 .

## Instructions

The numbers in bold face refer to the temperature either in degrees Celsius ( ${ }^{\circ} \mathrm{C}$ ) or Fahrenheit ( ${ }^{\circ} \mathrm{F}$ ) to convert into the other scale. If converting from ${ }^{\circ} \mathrm{F}$ to ${ }^{\circ} \mathrm{C}$, the equivalent temperature will be found in the left column. If converting from degrees ${ }^{\circ} \mathrm{C}$ to degrees ${ }^{\circ} \mathrm{F}$, the answer will be found in the column to the right.

| ${ }^{\circ} \mathrm{C}$ | -50 to 45 | ${ }^{\circ} \mathrm{F}$ |
| :---: | :---: | :---: |
| -45.6 | -50 | -58 |
| -40.0 | -40 | -40 |
| -34.4 | -30 | -22 |
| -28.9 | -20 | -4 |
| -23.3 | -10 | 14 |
| -17.8 | 0 | 32 |
| -17.2 | 1 | 33.8 |
| -16.7 | 2 | 35.6 |
| -16.1 | 3 | 37.4 |
| -15.6 | 4 | 39.2 |
| -15.0 | 5 | 41.0 |
| -14.4 | 6 | 42.8 |
| -13.9 | 7 | 44.6 |
| -13.3 | 8 | 46.4 |
| -12.8 | 9 | 48.2 |
| -12.2 | 10 | 50.0 |
| -11.7 | 11 | 51.8 |
| -11.1 | 12 | 53.6 |
| -10.6 | 13 | 55.4 |
| -10.0 | 14 | 57.2 |
| -9.44 | 15 | 59.0 |
| -8.89 | 16 | 60.8 |
| -8.33 | 17 | 62.6 |
| -7.78 | 18 | 64.4 |
| -7.22 | 19 | 66.2 |
| -6.67 | 20 | 68.0 |
| -6.11 | 21 | 69.8 |
| -5.56 | 22 | 71.6 |
| -5.00 | 23 | 73.4 |
| -4.44 | 24 | 75.2 |
| -3.89 | 25 | 77.0 |
| -3.33 | 26 | 78.8 |
| -2.78 | 27 | 80.6 |
| -1.67 | 28 | 82.4 |
| -1.67 | 29 | 84.2 |
| -1.11 | 30 | 86.0 |
| -0.56 | 31 | 87.8 |
| 0 | 32 | 89.6 |
| 0.56 | 33 | 91.4 |
| 1.11 | 34 | 93.2 |
| 1.67 | 35 | 95.0 |
| 2.22 | 36 | 96.8 |
| 2.78 | 37 | 98.6 |
| 3.33 | 38 | 100.4 |
| 3.89 | 39 | 102.2 |
| 4.44 | 40 | 104.0 |
| 5.00 | 41 | 105.8 |
| 5.56 | 42 | 107.6 |
| 6.11 | 43 | 109.4 |
| 6.67 | 44 | 111.2 |
| 7.22 | 45 | 113.0 |


| ${ }^{\circ} \mathrm{C}$ | 46 to 96 | ${ }^{\circ} \mathrm{F}$ |
| :---: | :---: | :---: |
| 7.78 | 46 | 114.8 |
| 8.33 | 47 | 116.6 |
| 8.89 | 48 | 118.4 |
| 9.44 | 49 | 120.2 |
| 10.0 | 50 | 122.0 |
| 10.6 | 51 | 123.8 |
| 11.1 | 52 | 125.6 |
| 11.7 | 53 | 127.4 |
| 12.2 | 54 | 129.2 |
| 12.8 | 55 | 131.0 |
| 13.3 | 56 | 132.8 |
| 13.9 | 57 | 134.6 |
| 14.4 | 58 | 136.4 |
| 15.0 | 59 | 138.2 |
| 15.6 | 60 | 140.0 |
| 16.1 | 61 | 141.8 |
| 16.7 | 62 | 143.6 |
| 17.2 | 63 | 145.4 |
| 17.8 | 64 | 147.2 |
| 18.3 | 65 | 149.0 |
| 18.9 | 66 | 150.8 |
| 19.4 | 67 | 152.6 |
| 20.0 | 68 | 154.4 |
| 20.6 | 69 | 156.2 |
| 21.1 | 70 | 158.0 |
| 21.7 | 71 | 159.8 |
| 22.2 | 72 | 161.6 |
| 23.8 | 73 | 163.4 |
| 23.3 | 74 | 165.2 |
| 23.9 | 75 | 167.0 |
| 21.1 | 76 | 168.8 |
| 25.0 | 77 | 170.6 |
| 25.6 | 78 | 172.4 |
| 26.1 | 79 | 174.2 |
| 26.7 | 80 | 176.0 |
| 27.2 | 81 | 177.8 |
| 27.8 | 82 | 179.6 |
| 28.3 | 83 | 181.4 |
| 28.9 | 84 | 183.2 |
| 29.4 | 85 | 185.0 |
| 30.0 | 86 | 186.8 |
| 30.6 | 87 | 188.6 |
| 31.1 | 88 | 190.4 |
| 31.7 | 89 | 192.2 |
| 32.2 | 90 | 194.0 |
| 32.8 | 91 | 195.8 |
| 33.3 | 92 | 197.6 |
| 33.9 | 93 | 199.4 |
| 34.4 | 94 | 201.2 |
| 35.0 | 95 | 203.0 |
| 35.6 | 96 | 204.8 |


| ${ }^{\circ} \mathrm{C}$ | 97 to 1000 | ${ }^{\circ} \mathrm{F}$ |
| :---: | :---: | :---: |
| 36.1 | 97 | 206.6 |
| 36.7 | 98 | 208.4 |
| 37.2 | 99 | 210.2 |
| 37.8 | 100 | 212.0 |
| 43 | 110 | 230 |
| 49 | 120 | 248 |
| 54 | 130 | 266 |
| 60 | 140 | 284 |
| 66 | 150 | 302 |
| 71 | 160 | 320 |
| 77 | 170 | 338 |
| 82 | 180 | 356 |
| 88 | 190 | 374 |
| 93 | 200 | 392 |
| 99 | 210 | 410 |
| 100 | 212 | 413 |
| 104 | 220 | 426 |
| 110 | 230 | 443 |
| 116 | 240 | 464 |
| 121 | 250 | 482 |
| 127 | 260 | 500 |
| 132 | 270 | 518 |
| 138 | 280 | 536 |
| 143 | 290 | 554 |
| 149 | 300 | 572 |
| 154 | 310 | 590 |
| 160 | 320 | 608 |
| 166 | 330 | 626 |
| 171 | 340 | 644 |
| 177 | 350 | 662 |
| 182 | 360 | 680 |
| 188 | 370 | 698 |
| 193 | 380 | 716 |
| 199 | 390 | 734 |
| 204 | 400 | 752 |
| 210 | 410 | 770 |
| 216 | 420 | 788 |
| 221 | 430 | 806 |
| 227 | 440 | 824 |
| 232 | 450 | 842 |
| 238 | 460 | 860 |
| 243 | 470 | 878 |
| 249 | 480 | 896 |
| 254 | 490 | 914 |
| 260 | 500 | 932 |
| 316 | 600 | 1112 |
| 371 | 700 | 1292 |
| 427 | 800 | 1472 |
| 482 | 900 | 1652 |
| 538 | 1000 | 1832 |




[^0]:    * This equates to a pump head pressure of approximately 230 ft . Not very common HVAC applications.
    ** Valve can be line sized to minimize pressure losses; butterfly valves are also used for these applications.

